

# Visible Light Wireless Communications

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Introduction

LEDs and  
photo diodes

VLC  
characteristics

MIMO,  
OFDM, QCM,  
DCM in VLC

VLC with  
lighting  
constraints

Outdoor VLC,  
VLC attocells

Concluding  
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# Wireless spectrum

Introduction

LEDs and photo diodes

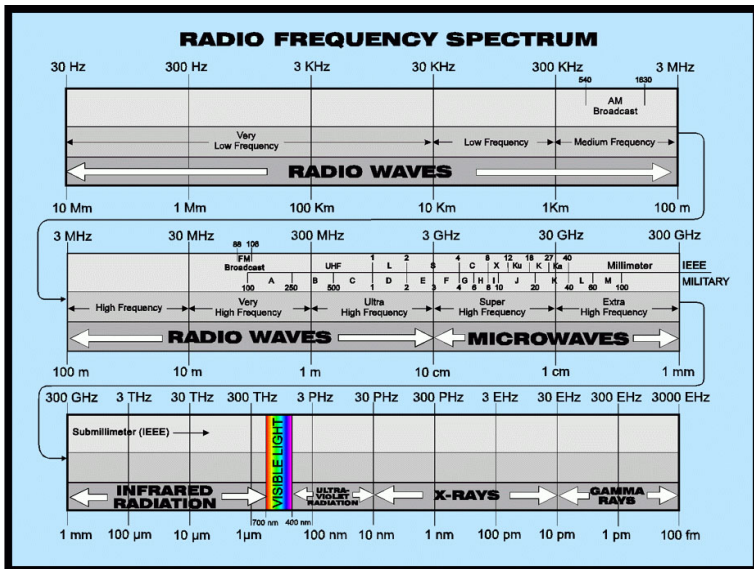
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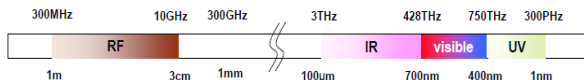
Outdoor VLC, VLC attocells

Concluding remarks



Source: Internet

- Optical wireless communication (OWC)
  - promising complementary technology for RF communication (RFC) technology
  - information conveyed via **optical radiation in free space**
  - wavelengths of interest
    - infrared to ultraviolet
    - includes **visible light** wavelengths (380 to 780 nm)



Source: [www.ieee802.org/15](http://www.ieee802.org/15)

- Visible light communication (VLC)
  - **communications using visible light spectrum**
  - abundant VLC spectrum (**~ 300 THz bandwidth**)
  - **multi-gigabit rates** over short distances
  - **LEDs as transmitters** and **photo diodes (PD) as receivers**

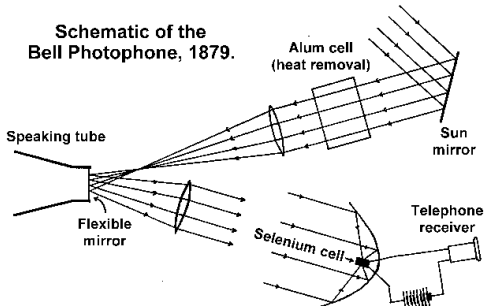
- Pros

- low power, low cost devices (LEDs, PDs)
- no spectrum cost
- no RF radiation issues
- inherent security in closed-room applications
- simultaneous data transmission and lighting
  - VLC technology rides along with efficient white LED lighting technology
- MIMO and OFDM techniques
  - improve spectral efficiency and performance

- Cons

- channel itself!
  - ambient light/interference from other light sources
  - alignment between Tx and Rx
  - scattering and multipath dispersion (ISI)
- no/low mobility

- 1879: 'photophone' by Alexander G. Bell  
(Patented Dec. 14, 1880. Filing date: Sep. 25, 1880. Patent No. US235496 A. Title: Photophone-Transmitter)
- Analog voice transceiver
- Transmitter: a mirror controls the amount of light reflected from a source
- Receiver: a photocell connected to a speaker



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- 1980
  - infrared remote controls (analog)
- 1993
  - infrared data transfer in mobiles, laptops, etc.
  - standards body: IrDA (9.6-128 Kbps).
- IEEE 802.15c
  - low power, high data rate systems in satellites, portable devices, etc.
- VLCC: Visible Light Communication Consortium
- VLC for home networks
  - hOME Gigabit Access (OMEGA) project
- IEEE 802.15.7
  - VLC PHY, up to 96 Mbps
- LiFi and attocells

# VLC implementations/applications

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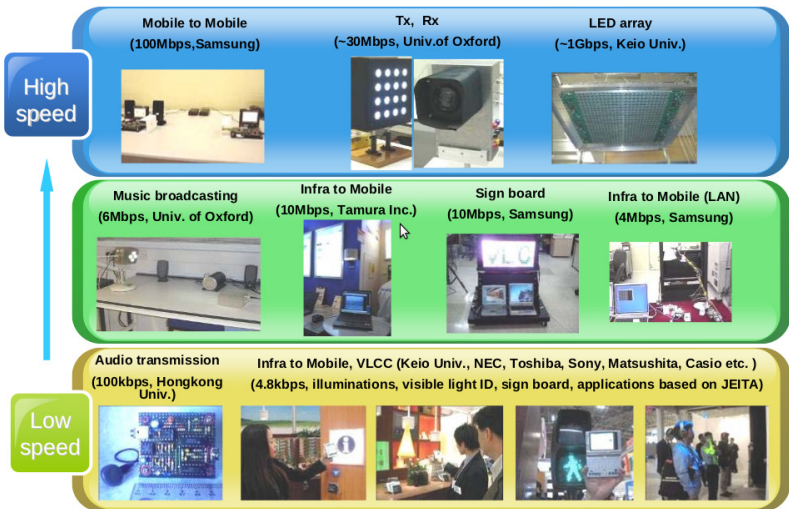
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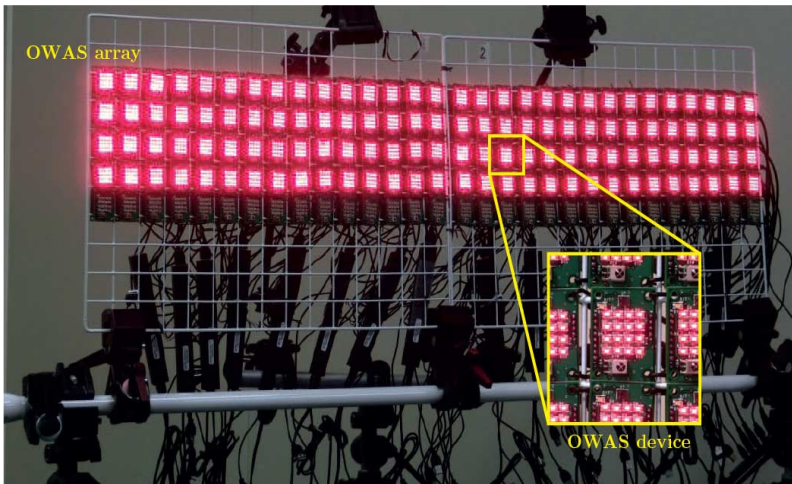
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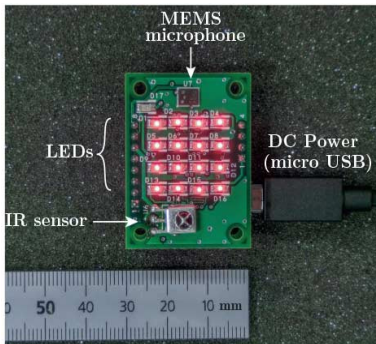
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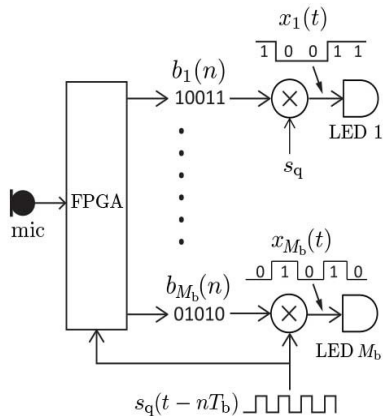
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(a)



(b)

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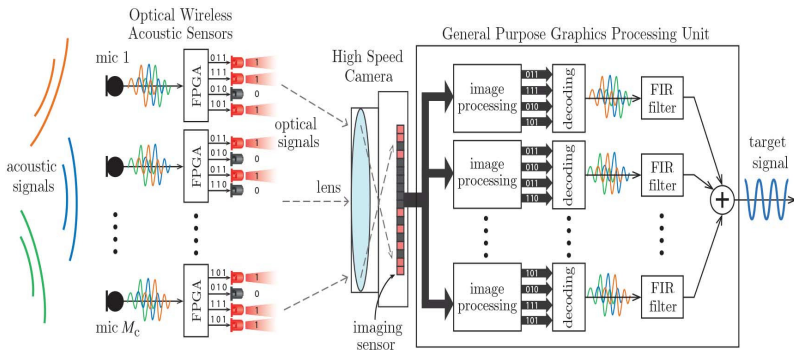
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# LEDs and photo diodes

# Why LEDs?

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  - measure of the quantity of visible light emitted by a source
  - example LED specs: 5 lumens, 90 lumens, 160 lumens

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  - **LED lamp**: **90 lumens/watt** (1 W for 90 lm)
  - High pressure sodium vapour lamp: **117 lumens/watt** (0.77 W for 90 lm)

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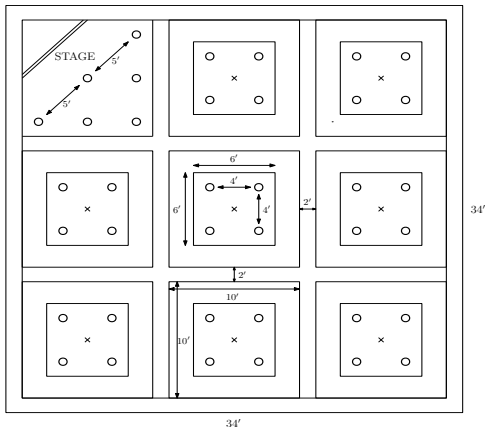
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  - **examples commercial white LED spec: 90 lm/W, 120 lm/W**

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- Target for 2020: 200 lm/W
  - claimed to have been breached! **208 lm/W LED** (prototype)

- Lighting arrangement in Golden Jubilee Seminar Hall, ECE



- Off-stage
  - 32 bulbs (20 W bulbs previously; now replaced with 5 W LED bulbs)
- On-stage
  - 6 bulbs (60 W bulbs previously; now replaced with 18 W LED bulbs)

## Luminous intensity (LI):

- Luminous power radiated by a point light source in a particular direction **per unit solid angle**
- SI unit of LI: Candela (Lumens/Steradian); cd (lm/sr)

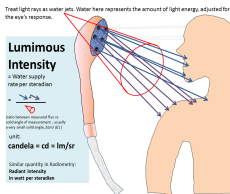


Image source: Wikipedia

- Solid angle (in steradians) of a cone with apex angle  $\theta$  (in degrees) =  $2\pi(1 - \cos \frac{\theta^\circ}{2})$ , i.e., **cd = lm/( $2\pi(1 - \cos \frac{\theta^\circ}{2})$ )**
- Examples of white LED spec:**
  - Luminous flux = 90 lm; luminous intensity = 59 cd  
 $\Rightarrow \theta = 81.5^\circ$  (viewing angle at 50% power; half-power angle)
  - Luminous intensity = 59 cd;  $\theta = 55^\circ$   
 $\Rightarrow$  **Luminous flux = 41.8 lm**
  - luminous intensity = 11200 mcd (11.2 cd);  $\theta = 45^\circ$   
 $\Rightarrow$  **Luminous flux = 5.35 lm**

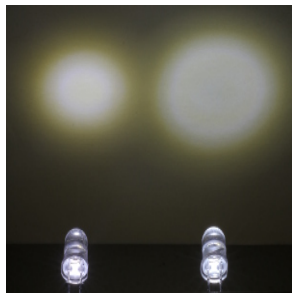
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- Luminous intensity (LI):
  - Two LEDs with same luminous flux of 0.2 lumens
  - Left LED's solid angle is  $15^\circ$ .  $\implies LI = 3.7 \text{ cd}$
  - Right LED's solid angle is  $30^\circ$ .  $\implies LI = 0.9 \text{ cd}$
  - Left LED produces a smaller, brighter spot



(a)



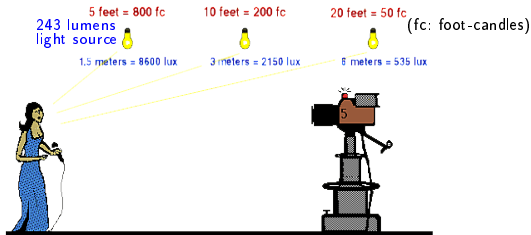
(b)

Image source: Internet



- **Illuminance:**

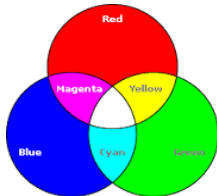
- measure of how much luminous power is incident on a given area
- **brightness:** subjective impression of illuminance
- SI unit of illuminance: **Lux** (lx)
- Lux: Lumens per square meter ( $\text{lm}/\text{m}^2$ )
- illuminance varies inversely with square of the distance from the source in free-space line of sight
  - Luminous flux (lumens) = Illuminance (lx)  $\times 4\pi r^2$   
( $r$ : distance from source in meters)



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- Color temperature:
  - different shades of white



- 'yellowish white' (warm white): 2700° K
- 'bluish white' (cool white): 6000° K



Image source: Internet

- **Color rendering index (CRI):**
  - a measure of a light source's ability to show object colors 'realistically' (or 'naturally') compared to a familiar reference source, either incandescent light or daylight
  - **Max. value is 100**
  - Lower CRI values
    - ⇒ some colors may appear unnatural when illuminated by the light source (LED) in question
  - Example CRI values:
    - 70-80 (cool LED); 80-90 (warm/neutral LED)
- **Switching speed (rise/fall times):**
  - **typ. tens of nsec**
  - switch LED for the following reasons:
    - to meet **illumination constraints (dimming)**
      - consider human eye's response characteristics
    - to achieve **data communication**
      - consider photo detector's response characteristics
    - to achieve both dimming control and communication simultaneously

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- White LED spectrum:

- Emitted wavelengths of a white LED include peaks in blue (450-470 nm) and yellow (570-590 nm) regions (solid curve)
- Interpreted as white light by the human eye
  - Relative light sensitivity of human eye is shown (dotted curve)

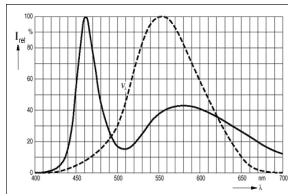


Image source: Internet

- Half-power semi-angle,  $\Phi_{\frac{1}{2}}$ :

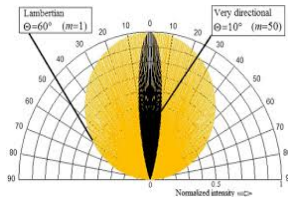
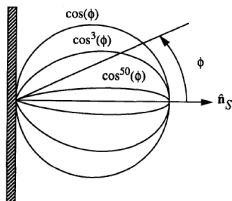


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$$R(\phi) = \frac{n+1}{2\pi} P_S \cos^n(\phi) \quad \text{for } \phi \in \left[-\frac{\pi}{2}, \frac{\pi}{2}\right]$$

### Generalized Lambertian radiation pattern of LED

- $n$  is the mode number of the radiating lobe given by

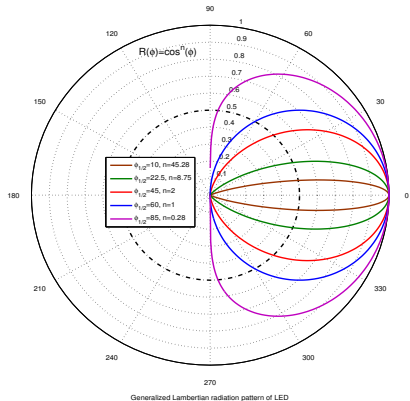
$$n = \frac{-\ln(2)}{\ln \cos \Phi_{\frac{1}{2}}}, \quad \Phi_{\frac{1}{2}} \text{ is half-power semi-angle}$$

- Mode number specifies the directionality of the source
  - larger the mode number, higher is the directionality
  - $n = 1$  corresponds to a traditional Lambertian source

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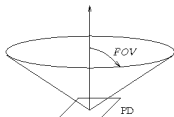
- Generalized Lambertian radiation pattern



- Flicker

- Fluctuation of the brightness of light (as perceived by human eye)
- LEDs are switched for the purposes of
  - ① communication (using intensity modulation, e.g., OOK/PAM)
  - ② dimming control (e.g., PWM)
- Human eye won't perceive flicker frequency  $> 200$  Hz
- No perceived flicker as long as the signaling rate is  $> 200$  Hz (i.e., one signaling interval  $< 5$  ms)
- Communication signaling rates are often much higher than 200 Hz
- So VLC using intensity modulation is not a major source of flicker

- Photo diode
  - Semiconductor (e.g., Si, Ge) device that converts light into current (may contain optical filters, built-in lenses)
- Key specifications
  - **Responsivity**: Amperes/Watt
    - ratio of the generated photo current to incident light power
  - **Response/rise time ( $t_r$ )**:
    - determined by resistance and capacitance of the photo diode and external circuitry (typ. tens of nsec)
    - **determines the bandwidth available for signal modulation ( $f_{bw}$ ) and thus data transmission**
  - **Modulation signal bandwidth**:
    - $f_{bw} = \frac{0.35}{t_r}$ ; e.g.,  $t_r = 50 \text{ ns} \Rightarrow f_{bw} = 7 \text{ MHz}$
  - **Field of view (FOV)**: angle (e.g.,  $85^\circ$ )
    - only the rays coming within FOV create response





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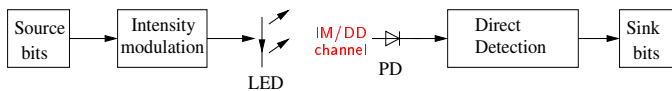
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- RF communication
  - Transmitter
    - Tx RF chain (up converter, power amplifier), Tx antenna
  - Receiver
    - Rx antenna, Rx RF chain (low noise amplifier, down converter)
- VLC
  - Transmitter
    - LED
    - Tx data by intensity modulating (IM) the LED
  - Receiver
    - Photo detector
    - Rx data by direct detection (DD)
  - LEDs/PDs with fast switching times
    - rise and fall times typ. tens of nsec

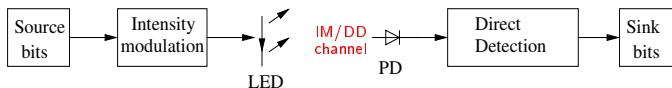
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- VLC Tx-Rx



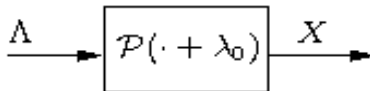
- VLC Tx-Rx



- IM/DD channel

- Modeled using Poisson processes to account for the quantum nature of light
  - channel output (i.e., the detected number of photons) is a r. v. which has a Poisson distribution with parameter  $\lambda$
  - $\lambda$  corresponds to the expected received intensity level
- Signal independent noise
  - originates from background radiation from other light sources (day/ambient light, fluorescent lamps, etc.) and
  - electronics in the receiver (thermal noise)
- Signal dependent noise
  - high-brightness LEDs where the randomness in the signal itself can not be neglected

- **Poisson channel** (memoryless, discrete-time)
  - Derived from photon-counting (hence the Poisson nature)
  - Input: r.v  $\Lambda \geq 0$
  - Output: discrete r.v  $X$  drawn from Poisson distribution with parameter  $\Lambda + \lambda_0$ , i.e.,  $X \sim \mathcal{P}(\Lambda + \lambda_0)$



- Non-negative term  $\lambda_0$ :
  - a constant related to ambient light or thermal noise
- Conditional output probability of this channel is

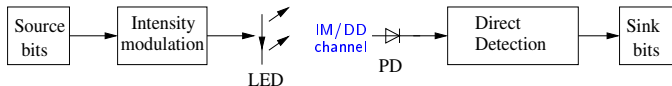
$$p(x|\lambda) = e^{-(\lambda+\lambda_0)} \frac{(\lambda + \lambda_0)^x}{x!}, \quad x \in \mathbb{N}, \quad \lambda \geq 0$$

- Distribution of r.v.  $X \sim \mathcal{P}(\lambda)$  for large  $\lambda$  approaches a Gaussian distribution  $\mathcal{N}(\lambda, \lambda)$

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- VLC Tx-Rx



- Baseband communication (no passband involved)
- Signaling: positive, real-valued tx. signals

D.C.O'Brien *et al*, "Visible light communications: challenges and possibilities", *IEEE PIMRC'2008*.

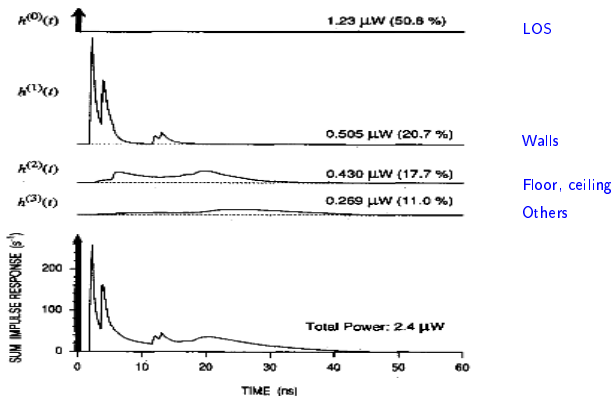
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- CIR between source  $\mathcal{S}$  and receiver  $\mathcal{R}$  at time  $t$  is given by

$$h(t; \mathcal{S}, \mathcal{R}) = \sum_{k=0}^{\infty} h^{(k)}(t; \mathcal{S}, \mathcal{R})$$

$h^{(k)}(t)$ : response of light undergoing exactly  $k$  reflections



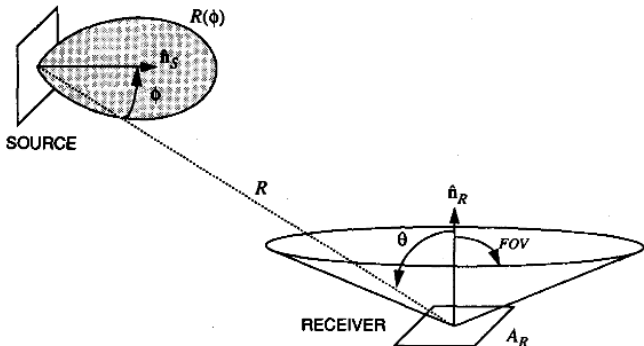
J. Barry *et al*, "Simulation of multipath impulse response for indoor wireless optical channels," *IEEE J. Sel. Areas in Commun.*, vol. 11, no. 3, pp. 367-379, Apr. 1993.

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- $h_{ij}$ : LOS channel gain between  $j$ th LED and  $i$ th PD is

$$h_{ij} = \frac{n+1}{2\pi} \cos^n \phi \cos \theta \frac{A}{R^2} \text{rect}\left(\frac{\theta}{\text{FOV}}\right)$$



Geometry of LED source and photo detector



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# MIMO in VLC

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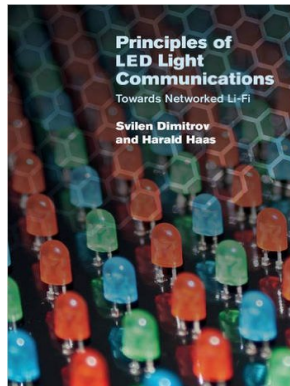
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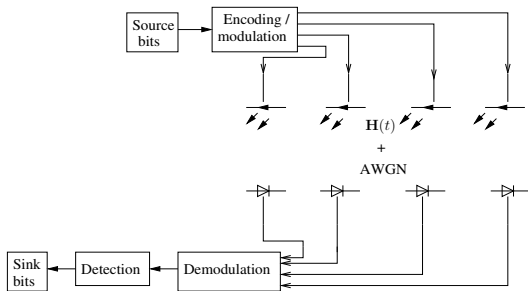
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- Multiple LEDs and PDs
- $N_t$ : no. of LEDs at Tx;  $N_r$ : no. of PDs at Rx



4 × 4 MIMO VLC

- Advantages
  - high data rates ( $N_t$  symbols per channel use)
  - gives MIMO gains even under LOS conditions
  - induced power imbalance at Tx LEDs helps

# A typical indoor VLC configuration

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LEDs and photo diodes

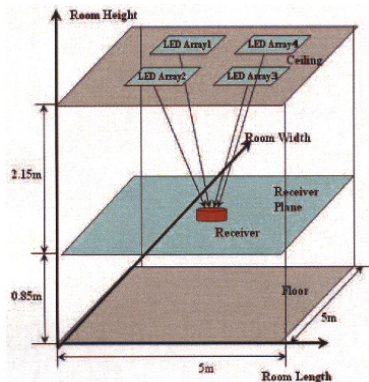
VLC characteristics

MIMO, OFDM, QCM, DCM in VLC

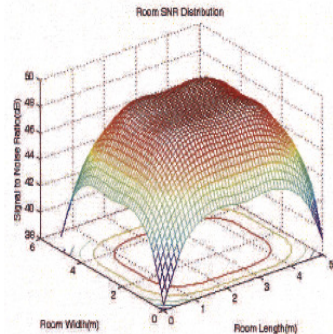
VLC with lighting constraints

Outdoor VLC, VLC attocells

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(g) Typical indoor VLC configuration



(h) SNR as a function of receiver position

D.C.O'Brien *et al*, "Visible light communications: challenges and possibilities", [IEEE PIMRC'2008](#).

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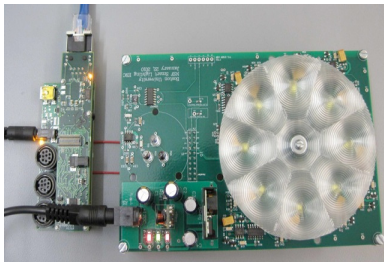
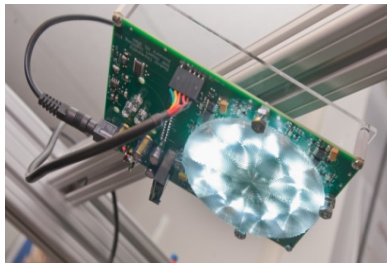
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- $8 \times 8$  MIMO VLC system



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- 48-LED array



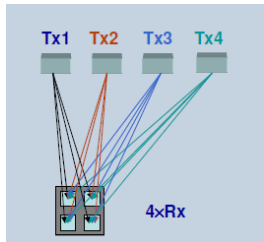
Source: Internet

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- $N_t$  LEDs (transmitter)
- $N_r$  photo detectors (receiver)
- $\mathbf{H}$  denotes the  $N_r \times N_t$  VLC MIMO channel matrix

$$\mathbf{H} = \begin{bmatrix} h_{11} & h_{12} & h_{13} & \cdots & h_{1N_t} \\ h_{21} & h_{22} & h_{23} & \cdots & h_{2N_t} \\ \vdots & \vdots & \ddots & \vdots & \vdots \\ h_{N_r,1} & h_{N_r,2} & h_{N_r,3} & \cdots & h_{N_r,N_t} \end{bmatrix}$$



MIMO channel between LEDs and PDs

# Example VLC channel matrices

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- Channel matrix for  $d_{tx} = 1m$ 
  - Channel gain: High
  - Channel correlation: High

$$\mathbf{H}_{d_{tx}=1m} = \begin{bmatrix} 0.5600 & 0.5393 & 0.5196 & 0.5393 \\ 0.5393 & 0.5600 & 0.5393 & 0.5196 \\ 0.5196 & 0.5393 & 0.5600 & 0.5393 \\ 0.5393 & 0.5196 & 0.5393 & 0.5600 \end{bmatrix} \times 10^{-5}$$

- Channel matrix for  $d_{tx} = 4m$ 
  - Channel gain: Low
  - Channel correlation: Low

$$\mathbf{H}_{d_{tx}=4m} = \begin{bmatrix} 0.9947 & 0.9337 & 0.8782 & 0.9337 \\ 0.9337 & 0.9947 & 0.9337 & 0.8782 \\ 0.8782 & 0.9337 & 0.9947 & 0.9337 \\ 0.9337 & 0.8782 & 0.9337 & 0.9947 \end{bmatrix} \times 10^{-6}$$



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- Transmit signals in VLC must be
  - **positive real-valued** for intensity modulation of LEDs
- Approaches
  - OOK
  - $M$ -PAM with positive signal points
  - $M$ -QAM/ $M$ -PSK with Hermitian symmetry
  - **SSK** and **spatial modulation** using multiple LEDs
  - **QCM, DCM** (Quad-/Dual-LED complex modulation)

T. Fath and H. Haas, "Performance comparison of MIMO techniques for optical wireless communications in indoor environments," *IEEE Trans. Commun.*, vol. 61, no. 2, pp. 733-742, Feb. 2013.

S. P. Alaka, T. Lakshmi Narasimhan, and A. Chockalingam, "Generalized spatial modulation in indoor wireless visible light communication," *IEEE GLOBECOM'2015*, San Diego, USA, Dec. 2015.

R. Tejaswi, T. Lakshmi Narasimhan, A. Chockalingam, "Quad-LED complex modulation (QCM) for visible light wireless communications" *IEEE WCNC'16 Workshop on Opt. Wireless Commun.*, Apr. 2016.

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- Spatial multiplexing (SMP)
  - $N_t$  LEDs and  $N_r$  PDs
  - At any given time, all LEDs are ON
  - $\eta_{smp} = N_t \log_2 M$  bpcu
- Spatial modulation (SM)
  - At any given time, any one LED is ON
  - Other  $N_t - 1$  LEDs are OFF
  - $\eta_{sm} = \lfloor \log_2 N_t \rfloor + \log_2 M$  bpcu
- Space shift keying (SSK)
  - Special case of SM
  - Only index of active LED conveys information
  - $\eta_{ssk} = \lfloor \log_2 N_t \rfloor$  bpcu

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- Generalized space shift keying (GSSK)
  - Generalization of SSK
  - $N_a \leq N_t$  active LEDs
  - $\eta_{gssk} = \lfloor \log_2 \binom{N_t}{N_a} \rfloor$  bpcu
- Generalized spatial modulation (GSM)
  - Generalization of SM
  - $N_a \leq N_t$  active LEDs
  - $\eta_{gsm} = \lfloor \log_2 \binom{N_t}{N_a} \rfloor + N_a \lfloor \log_2 M \rfloor$  bpcu

T. Fath and H. Haas, "Performance comparison of MIMO techniques for optical wireless communications in indoor environments," *IEEE Trans. Commun.*, vol. 61, no. 2, pp. 733-742, Feb. 2013.

S. P. Alaka, T. Lakshmi Narasimhan, and A. Chockalingam, "Generalized spatial modulation in indoor wireless visible light communication," *IEEE GLOBECOM'2015*, San Diego, USA, Dec. 2015.

- Each active LED emits an  $M$ -ary intensity modulation symbol  $I_m \in \mathbb{M}$ 
  - $\mathbb{M}$ : set of all possible intensity levels given by

$$I_m = \frac{2I_{p,m}}{M+1}, \quad m = 1, 2, \dots, M, \quad M = |\mathbb{M}|$$

- $\mathbf{x}$ :  $N_t \times 1$  transmit signal vector;  $x_i \in \{\mathbb{M} \cup 0\}$
- $\mathbf{n}$ :  $N_r \times 1$  noise vector at the receiver;  $n_i \sim \mathcal{N}(0, \sigma^2)$
- $\mathbf{n}$ :  $N_r \times 1$  received signal vector at the receiver

$$\mathbf{y} = \mathbf{a}\mathbf{H}\mathbf{x} + \mathbf{n}$$

$\mathbf{a}$ : responsivity of the PD (amp/Watt)

- Average received SNR

$$\bar{\gamma} = \frac{a^2 P_r^2}{\sigma^2}, \quad P_r^2 = \frac{1}{N_r} \sum_{i=1}^{N_r} \mathbb{E}[|\mathbf{h}_i \mathbf{x}|^2]$$

$\mathbf{h}_i$ :  $i$ th row of  $\mathbf{H}$

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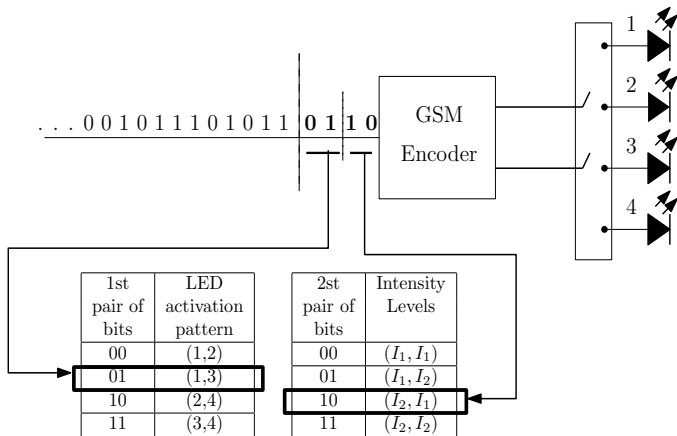
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GSM-MIMO transmitter for VLC system with  $N_t = 4$ ,  $N_a = 2$ ,  $M = 2$

- Intensity levels are  $I_1 = \frac{2}{3}$  and  $I_2 = \frac{4}{3}$
- We need **only 4 activation patterns** out of  $\binom{N_t}{N_a} = \binom{4}{2} = 6$  possible activation patterns
- So the GSM signal set for this example can be chosen as follows:

$$S_{N_t, M}^{N_a} = S_{4,2}^2 = \left\{ \begin{array}{l} \begin{bmatrix} \frac{2}{3} \\ \frac{2}{3} \\ 0 \\ 0 \end{bmatrix}, \begin{bmatrix} \frac{2}{3} \\ \frac{4}{3} \\ 0 \\ 0 \end{bmatrix}, \begin{bmatrix} \frac{4}{3} \\ \frac{2}{3} \\ 0 \\ 0 \end{bmatrix}, \begin{bmatrix} \frac{4}{3} \\ \frac{4}{3} \\ 0 \\ 0 \end{bmatrix}, \begin{bmatrix} \frac{2}{3} \\ 0 \\ \frac{2}{3} \\ 0 \end{bmatrix}, \begin{bmatrix} \frac{2}{3} \\ 0 \\ \frac{4}{3} \\ 0 \end{bmatrix}, \begin{bmatrix} \frac{4}{3} \\ 0 \\ \frac{2}{3} \\ 0 \end{bmatrix}, \begin{bmatrix} \frac{4}{3} \\ 0 \\ \frac{4}{3} \\ 0 \end{bmatrix}, \\ \begin{bmatrix} 0 \\ \frac{2}{3} \\ 0 \\ \frac{2}{3} \end{bmatrix}, \begin{bmatrix} 0 \\ \frac{2}{3} \\ 0 \\ \frac{4}{3} \end{bmatrix}, \begin{bmatrix} 0 \\ \frac{4}{3} \\ 0 \\ \frac{2}{3} \end{bmatrix}, \begin{bmatrix} 0 \\ \frac{4}{3} \\ 0 \\ \frac{4}{3} \end{bmatrix}, \begin{bmatrix} 0 \\ 0 \\ \frac{2}{3} \\ \frac{2}{3} \end{bmatrix}, \begin{bmatrix} 0 \\ 0 \\ \frac{2}{3} \\ \frac{4}{3} \end{bmatrix}, \begin{bmatrix} 0 \\ 0 \\ \frac{4}{3} \\ \frac{2}{3} \end{bmatrix}, \begin{bmatrix} 0 \\ 0 \\ \frac{4}{3} \\ \frac{4}{3} \end{bmatrix} \end{array} \right\}$$

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Maximum likelihood (ML) detection rule is

$$\hat{\mathbf{x}} = \underset{\mathbf{x} \in \mathbb{S}_{N_t, M}^{N_a}}{\operatorname{argmin}} \left( \frac{a}{\sigma} \|\mathbf{H}\mathbf{x}\|^2 - 2\mathbf{y}^T \mathbf{H}\mathbf{x} \right)$$

Pairwise error probability (PEP) is

$$PEP_{gsm} = Q \left( \frac{a}{2\sigma} \|\mathbf{H}(\mathbf{x}_2 - \mathbf{x}_1)\| \right)$$

Define  $L \triangleq |\mathbb{S}_{N_t, M}^{N_a}|$ . An upper bound on the BER for ML detection can be obtained using union bound as

$$\begin{aligned} BER_{gsm} &\leq \frac{1}{L} \sum_{i=1}^L \sum_{j=1, i \neq j}^{L-1} PEP(\mathbf{x}_i \rightarrow \mathbf{x}_j | \mathbf{H}) \frac{d_H(\mathbf{x}_i, \mathbf{x}_j)}{\eta_{gsm}} \\ &= \frac{1}{L} \sum_{i=1}^L \sum_{j=1, i \neq j}^{L-1} Q \left( \frac{r}{2\sigma} \|\mathbf{H}(\mathbf{x}_j - \mathbf{x}_i)\| \right) \frac{d_H(\mathbf{x}_i, \mathbf{x}_j)}{\eta_{gsm}} \end{aligned}$$

where  $d_H(\mathbf{x}_i, \mathbf{x}_j)$  is the Hamming distance between the bit mappings corresponding to the signal vectors  $\mathbf{x}_i$  and  $\mathbf{x}_j$

# Indoor VLC - A typical geometric set-up

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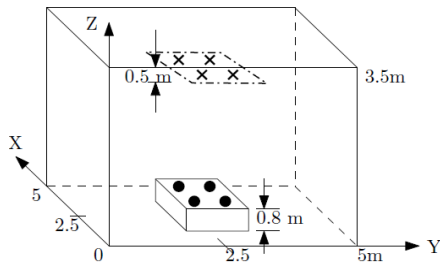
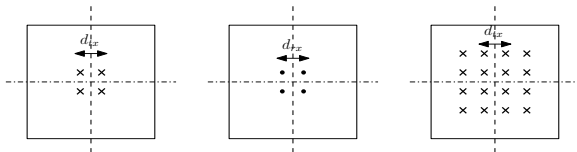


Figure : Geometric set-up of a typical indoor VLC system  
( $\times$  denotes an LED and  $\bullet$  denotes a PD)



(a)  $\mathbf{T_x}, N_t = 4$       (b)  $\mathbf{R_x}, N_r = 4$       (c)  $\mathbf{T_x}, N_t = 16$

Placement of LEDs and PDs



# System parameters

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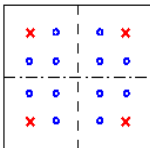
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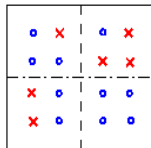
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|             |                       |                  |
|-------------|-----------------------|------------------|
| Room        | Length ( $X$ )        | 5m               |
|             | Width ( $Y$ )         | 5m               |
|             | Height ( $Z$ )        | 3.5m             |
| Transmitter | Height from the floor | 3m               |
|             | Elevation             | $-90^\circ$      |
|             | Azimuth               | $0^\circ$        |
|             | $\Phi_{1/2}$          | $60^\circ$       |
|             | Mode number, $n$      | 1                |
|             | $d_{tx}$              | 0.6m             |
| Receiver    | Height from the floor | 0.8m             |
|             | Elevation             | $90^\circ$       |
|             | Azimuth               | $0^\circ$        |
|             | Responsivity, $a$     | 0.75 Ampere/Watt |
|             | FOV                   | $85^\circ$       |
|             | $d_{rx}$              | 0.1m             |

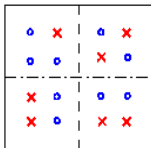
- LED placements in a  $4 \times 4$  square grid
- Different GSM configurations for  $\eta = 8$  bpcu, 5 bpcu



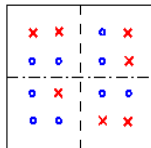
(d) GSM, 8 bpcu  
 $N_t = 4, N_a = 2, M = 8$



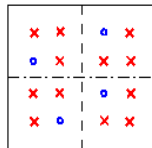
(e) GSM, 5 bpcu  
 $N_t = 6, N_a = 2, M = 2$



(f) GSM, 8 bpcu  
 $N_t = 7, N_a = 2, M = 4$



(g) GSM, 8 bpcu  
 $N_t = 7, N_a = 3, M = 2$



(h) GSM, 8 bpcu  
 $N_t = 12, N_a = 2, M = 2$

× indicates the presence of an LED. ○ indicates the absence of LED.

- Comparison of analytical upper bound and simulated BERs

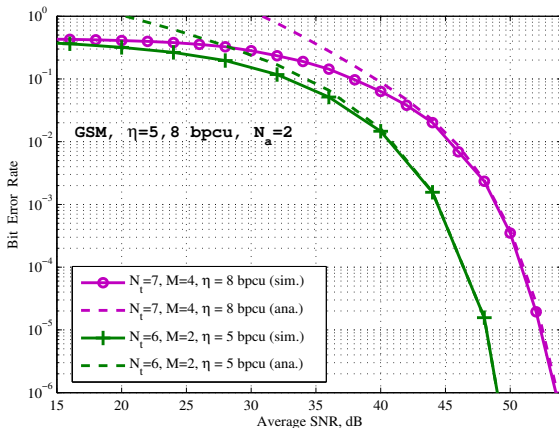


Figure : GSM with  $N_t = 6, 7$ ,  $N_a = 2$ ,  $M = 2, 4$ ,  $\eta_{gsm} = 5, 8$  bpcu.

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- Performance of different GSM configurations for fixed  $\eta = 8$  bpcu

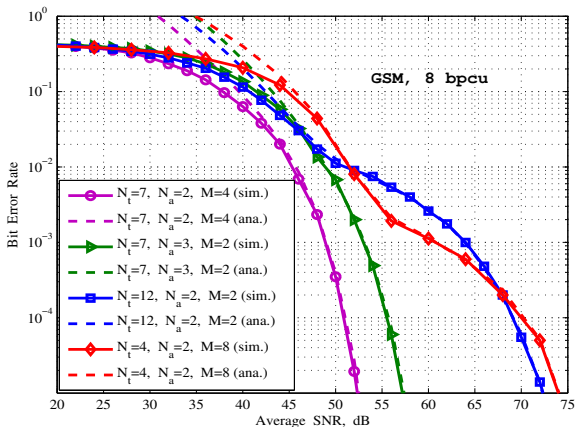


Figure : Comparison of the BER performance of different configurations of GSM with  $\eta_{gsm} = 8$  bpcu,  $N_r = 4$ .

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- Optimum placement of LEDs

- The minimum Euclidean distance between any two GSM signal vectors  $\mathbf{x}_1$  and  $\mathbf{x}_2$  transmitted through  $\mathbf{H}$  is given by

$$d_{\mathbf{H},min} \triangleq \min_{\mathbf{x}_1, \mathbf{x}_2 \in \mathbb{S}_{N_t, M}^{N_a}} \|\mathbf{H}(\mathbf{x}_2 - \mathbf{x}_1)\|^2$$

- Similarly, the average Euclidean distance between any two GSM signal vectors  $\mathbf{x}_1$  and  $\mathbf{x}_2$  transmitted through  $\mathbf{H}$  is

$$d_{\mathbf{H},avg} = \frac{1}{\binom{|\mathbb{S}_{N_t, M}^{N_a}|}{2}} \sum_{\mathbf{x}_1, \mathbf{x}_2 \in \mathbb{S}_{N_t, M}^{N_a}} \|\mathbf{H}(\mathbf{x}_2 - \mathbf{x}_1)\|^2$$

- Choose the placement of the LEDs at the transmitter such that  $d_{\mathbf{H},min}$  and  $d_{\mathbf{H},avg}$  are maximized over all possible placements

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| System | GSM configuration          | $d_{\mathbf{H},min}$    | $d_{\mathbf{H},avg}$    |
|--------|----------------------------|-------------------------|-------------------------|
| 1      | $N_t = 4, N_a = 2, M = 8$  | $4.623 \times 10^{-17}$ | $4.520 \times 10^{-11}$ |
| 2      | $N_t = 7, N_a = 2, M = 4$  | $1.977 \times 10^{-14}$ | $6.601 \times 10^{-11}$ |
| 3      | $N_t = 7, N_a = 3, M = 2$  | $1.541 \times 10^{-14}$ | $6.003 \times 10^{-11}$ |
| 4      | $N_t = 12, N_a = 2, M = 2$ | $1.346 \times 10^{-16}$ | $4.842 \times 10^{-11}$ |

Table : Values of  $d_{\mathbf{H},min}$  and  $d_{\mathbf{H},avg}$  for different GSM configurations with  $\eta_{gsm} = 8$  bpcu.

- Configuration 2 has the largest  $d_{\mathbf{H},min}$ ,  $d_{\mathbf{H},avg}$  and hence the best BER performance

# GSM performance for varying $d_{tx}$

- GSM performance as a function of  $d_{tx}$  for different SNRs

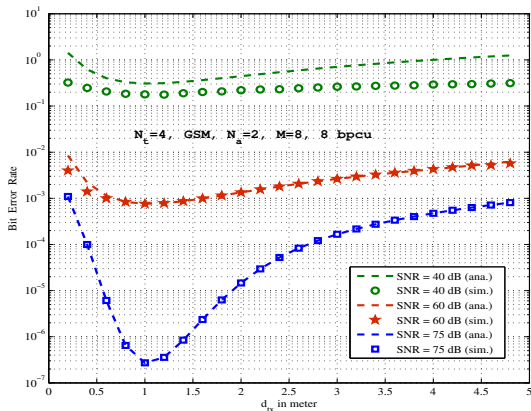


Figure : GSM with  $N_t = 4$ ,  $N_a = 2$ ,  $M = 8$ ,  $\eta_{gsm} = 8$  bpcu.

- Opposing effects of channel correlation and channel chains for increasing  $d_{tx}$  results in optimum  $d_{tx}$

# GSM vs other MIMO techniques

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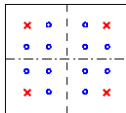
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- SMP, GSSK, SM, and GSM with  $\eta = 8$  bpcu

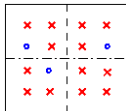
- **SMP:**

- $N_t = 4, N_a = 4, M = 4$



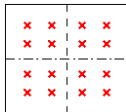
- **GSSK:**

- $N_t = 13, N_a = 3, M = 1$



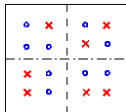
- **SM:**

- $N_t = 16, N_a = 1, M = 16$



- **GSM:**

- $N_t = 7, N_a = 2, M = 4$





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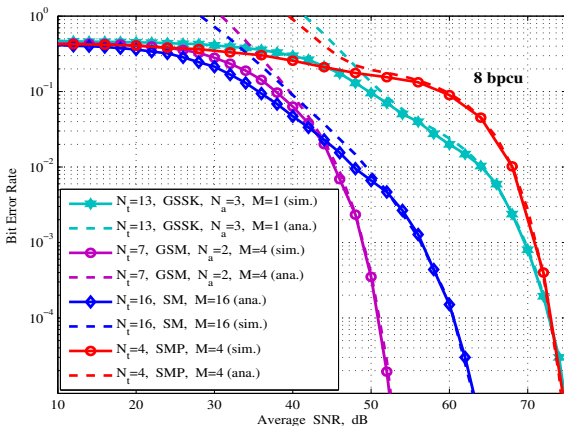
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- Comparison of the BER performance of SMP, GSSK, SM, and GSM for the same  $\eta = 8$  bpcu,  $N_r = 4$



- For the same  $\eta = 8$  bpcu, GSM performs better (by about 9 dB at  $10^{-5}$  BER) compared to SMP, SSK, GSSK, SM

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# OFDM in VLC

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- OFDM
  - Popular in wired and wireless RF communications
  - **Attractive in VLC as well**
- OFDM in RF communications
  - OFDM signals are in the complex domain
  - Signals can be bipolar
- OFDM in VLC
  - VLC transmit signal must be **real** and **positive**
  - Use **Hermitian symmetry** on information symbols before IFFT to obtain real signals
  - Perform bipolar or unipolar conversion
  - Achieves good performance (3 Gbps single-LED OFDM link has been reported)

J. Armstrong, "OFDM for optical communications," *J. Lightwave Tech.*, vol. 27, no. 3, pp. 89-204, Feb. 2009.

H. Elgala, R. Mesleh, H. Haas, and B. Pricope, "OFDM visible light wireless communication based on white LEDs," *Proc. IEEE VTC 2007-Spring*, pp. 2185-2189, Apr. 2007.

D. Tsonev et al, "A 3-Gb/s single-LED OFDM-based wireless VLC link using a gallium nitride  $\mu$ LED," *IEEE Photonics Tech. Lett.*, vol. 26, no. 7, pp. 637-640, Jan. 2014.

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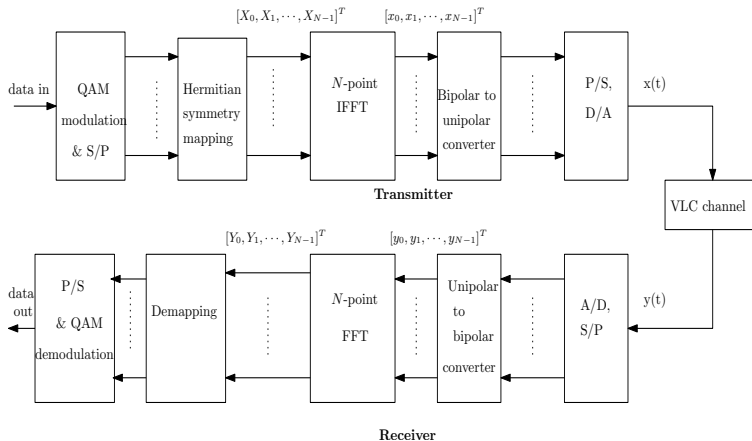


Figure : A general single-LED OFDM system model in VLC.

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- Techniques to generate VLC compatible OFDM signals in the positive real domain:
  - DCO OFDM (DC-biased optical OFDM)
  - ACO OFDM (Asymmetrically clipped optical OFDM)
  - Flip OFDM
  - NDC OFDM (Non-DC-biased OFDM)
  - CI-NDC OFDM (Coded Index NDC OFDM)

O. Gonzalez *et al*, "OFDM over indoor wireless optical channel," *Proc. IEE Optoelectronics*, vol. 152, no. 4, pp. 199-204, Aug. 2005.

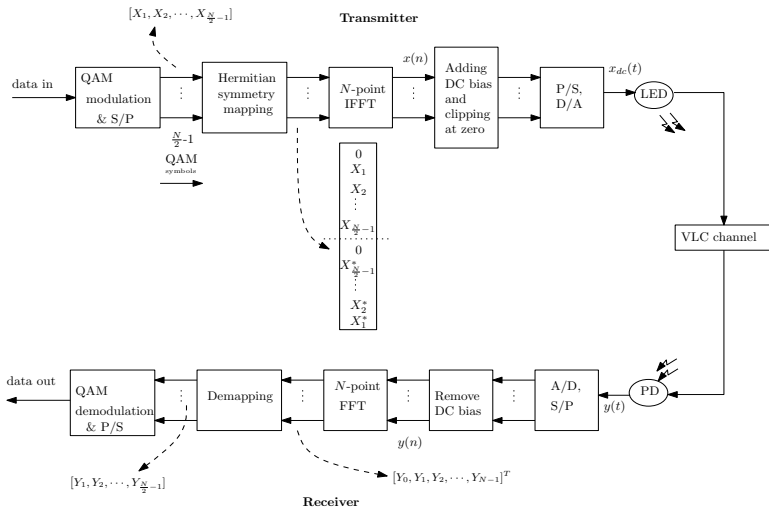
J. Armstrong and B. J. Schmidt, "Comparison of asymmetrically clipped optical OFDM and DC-biased optical OFDM in AWGN," *IEEE Commun. Letters*, vol. 12, no. 5, pp. 343-345, May 2008.

N. Fernando, Y. Hong, and E. Viterbo, "Flip-OFDM for unipolar communication systems," *IEEE Trans. Commun.*, vol. 60, no. 12, pp. 3726-3733, Aug. 2012.

Y. Li, D. Tsonev, and H. Haas, "Non-DC-biased OFDM with optical spatial modulation," *IEEE PIMRC 2013*, pp. 486-490, Sep. 2013.

S. P. Alaka, T. Lakshmi Narasimhan, and A. Chockalingam, "Coded index modulation for non-DC-biased OFDM in multiple LED visible light communication," *IEEE VTC 2016-Spring*, May 2016. 

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O. Gonzalez et al, "OFDM over indoor wireless optical channel," *Proc. IEEE Optoelectronics*, vol. 152, no. 4, pp. 199-204, Aug. 2005.

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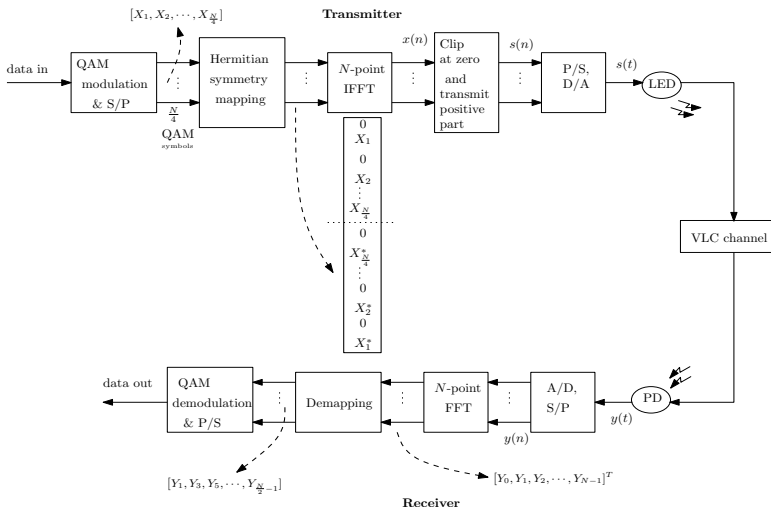
- $\frac{N}{2} - 1$  QAM symbols are modulated per OFDM symbol
- The unipolar OFDM signal  $x_{dc}(t)$  is given by

$$x_{dc}(t) = x(t) + B_{dc}$$

where  $x(t)$  is the bipolar OFDM signal

- $B_{dc} = k\sqrt{\mathbb{E}\{x^2(t)\}}$ ; define this as a bias of  $10 \log_{10}(k^2 + 1)$  dB
- The achieved rate in DCO OFDM is given by

$$\begin{aligned} \eta_{dco} &= \frac{\frac{N}{2} - 1}{N} \log_2 M \\ &\approx \frac{1}{2} \log_2 M \text{ bpcu, for large } N \end{aligned}$$



J. Armstrong and B. J. Schmidt, "Comparison of asymmetrically clipped optical OFDM and DC-biased optical OFDM in AWGN," *IEEE Commun. Letters*, vol. 12, no. 5, pp. 343-345, May 2008.



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- $\frac{N}{4}$  QAM symbols are modulated per OFDM symbol
- Only odd subcarriers are used to send information
- All even subcarriers are set to zero
- The unipolar OFDM signal is obtained by **clipping the negative signals at zero**
- The achieved data rate in ACO OFDM is given by

$$\eta_{aco} = \frac{1}{4} \log_2 M \text{ bpcu}$$

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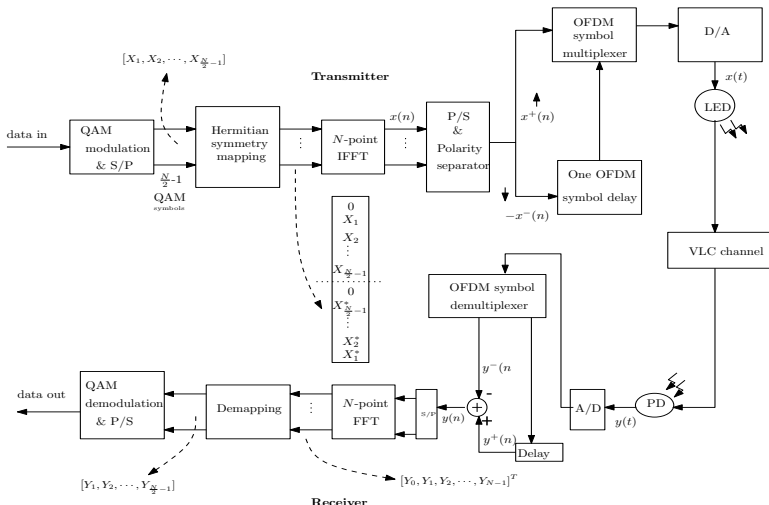
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N. Fernando, Y. Hong, and E. Viterbo, "Flip-OFDM for unipolar communication systems," *IEEE Trans. Commun.*, vol. 60, no. 12, pp. 3726-3733, Aug. 2012.

- $\frac{N}{2} - 1$  QAM symbols are modulated per OFDM symbol
- The unipolar OFDM signal is obtained by **flipping the negative signals**
- **Two OFDM time slots** are used to send one OFDM symbol
- Positive parts are sent on the first slot
- Flipped negative parts are sent on the second slot
- The achieved data rate in flip OFDM is given by

$$\begin{aligned}\eta_{flip} &= \frac{\frac{N}{2} - 1}{2N} \log_2 M \\ &\approx \frac{1}{4} \log_2 M \text{ bpcu, for large } N\end{aligned}$$

# DCO, ACO, flip OFDM performance

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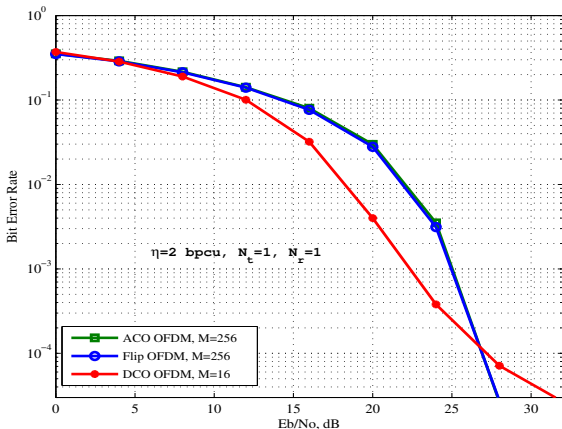


Figure : Comparison of the BER performance of ACO OFDM, flip OFDM, and DCO OFDM with 7dB bias for  $\eta = 2$  bpcu,  $N_t = N_r = 1$ .

# DCO OFDM performance for varying DC bias

- Optimum DC bias

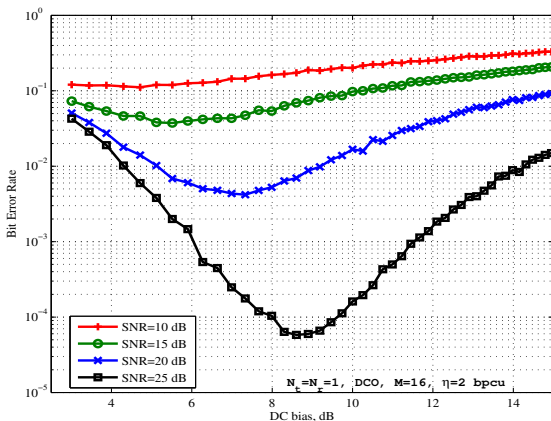


Figure : BER performance of DCO OFDM as a function of DC bias with  $\eta = 2$  bpcu,  $M = 16$ , and  $N_t = N_r = 1$ , for SNR = 10, 15, 20, 25 dB.

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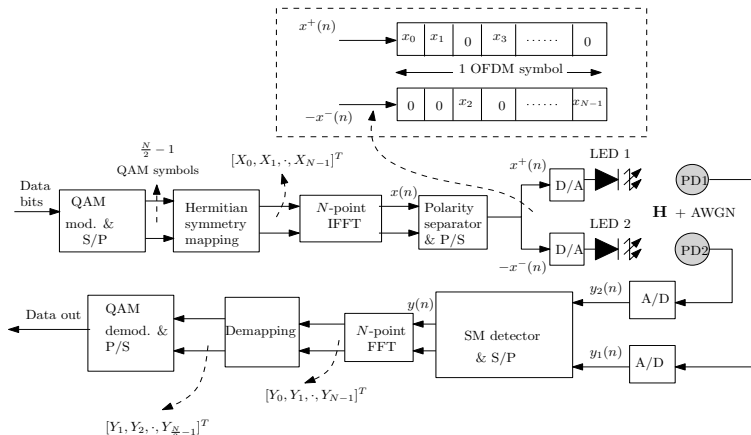
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- $$\eta_{ndc} = \frac{\frac{N}{2} - 1}{N} \log_2 M \approx \frac{1}{2} \log_2 M \text{ bpcu, for large } N$$

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- The detector output  $y(n)$ ,  $n = 0, 1, 2, \dots, N - 1$ , is

$$|y(n)| = \max_{i=1,2} |z_i(n)|$$

$$\text{sign}\{y(n)\} = \begin{cases} +\text{ve}, & \text{if } \arg \max_{i=1,2} |z_i(n)| = 1 \\ -\text{ve}, & \text{if } \arg \max_{i=1,2} |z_i(n)| = 2, \end{cases}$$

where

$$\begin{bmatrix} z_1(n) \\ z_2(n) \end{bmatrix} = \begin{bmatrix} (\mathbf{h}_1^T \mathbf{h}_1)^{-1} \mathbf{h}_1^T \mathbf{y} \\ (\mathbf{h}_2^T \mathbf{h}_2)^{-1} \mathbf{h}_2^T \mathbf{y} \end{bmatrix},$$

and  $\mathbf{h}_i$  is the  $i$ th column of channel matrix  $\mathbf{H}$ ,  $i = 1, 2$ .

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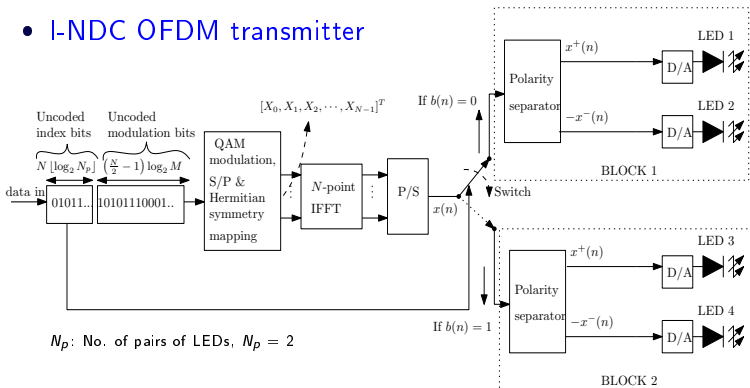
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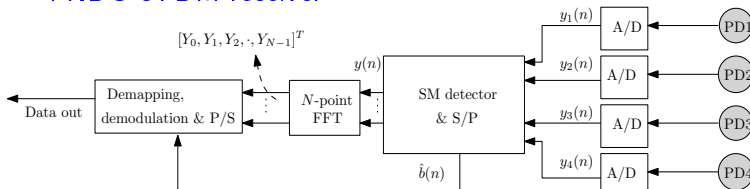
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## I-NDC OFDM transmitter



## I-NDC OFDM receiver





- The detector output  $y(n)$ ,  $n = 0, 1, 2, \dots, N - 1$ , is

$$|y(n)| = \max_{i=1,2,3,4} |z_i(n)|$$

$$\text{sign}\{y(n)\} = \begin{cases} +\text{ve,} & \text{if } \arg \max_{i=1,2,3,4} |z_i(n)| = 1 \\ -\text{ve,} & \text{if } \arg \max_{i=1,2,3,4} |z_i(n)| = 2 \\ +\text{ve,} & \text{if } \arg \max_{i=1,2,3,4} |z_i(n)| = 3 \\ -\text{ve,} & \text{if } \arg \max_{i=1,2,3,4} |z_i(n)| = 4, \end{cases}$$

where

$$\begin{bmatrix} z_1(n) \\ z_2(n) \\ z_3(n) \\ z_4(n) \end{bmatrix} = \begin{bmatrix} (\mathbf{h}_1^T \mathbf{h}_1)^{-1} \mathbf{h}_1^T \mathbf{y} \\ (\mathbf{h}_2^T \mathbf{h}_2)^{-1} \mathbf{h}_2^T \mathbf{y} \\ (\mathbf{h}_3^T \mathbf{h}_3)^{-1} \mathbf{h}_3^T \mathbf{y} \\ (\mathbf{h}_4^T \mathbf{h}_4)^{-1} \mathbf{h}_4^T \mathbf{y} \end{bmatrix},$$

and  $\mathbf{h}_i$  is the  $i$ th column of channel matrix  $\mathbf{H}$ ,  $i = 1, 2, 3, 4$ .

# Performance of NDC OFDM, I-NDC OFDM

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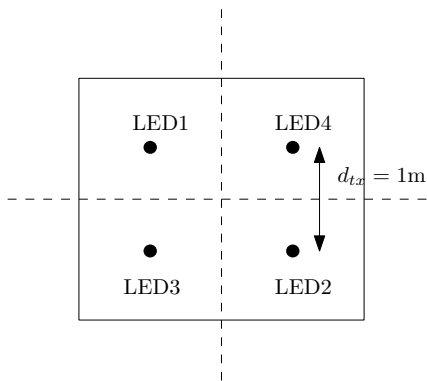
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- Placement of LEDs



- BLOCK 1: (LED1, LED2)
- BLOCK 2: (LED3, LED4)

# NDC OFDM and I-NDC OFDM performance

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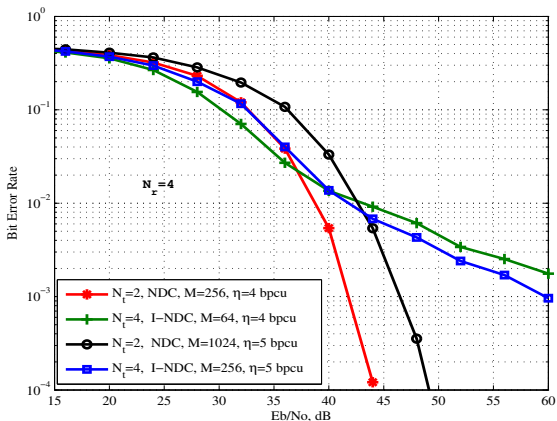


Figure : BER performance of I-NDC OFDM and NDC OFDM for  $\eta = 4, 5$  bpcu,  $N_r = 4$

# NDC OFDM and I-NDC OFDM performance

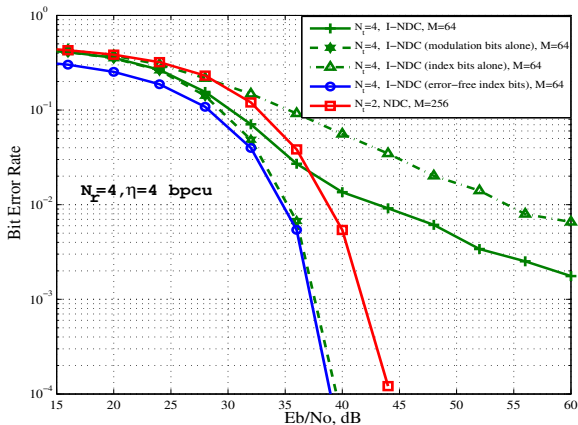


Figure : Reliability of modulation bits and index bits in I-NDC OFDM for  $\eta = 4$  bpcu,  $N_r = 4$

- Reliability of index bits is poor!
- Use coding for index bits

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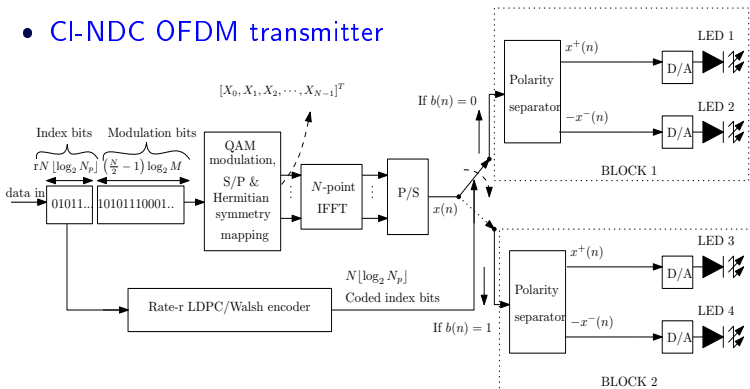
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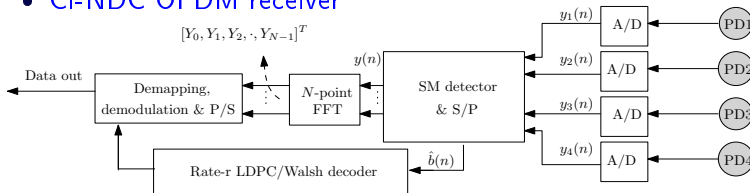
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## CI-NDC OFDM transmitter



## CI-NDC OFDM receiver



# CI-NDC OFDM performance

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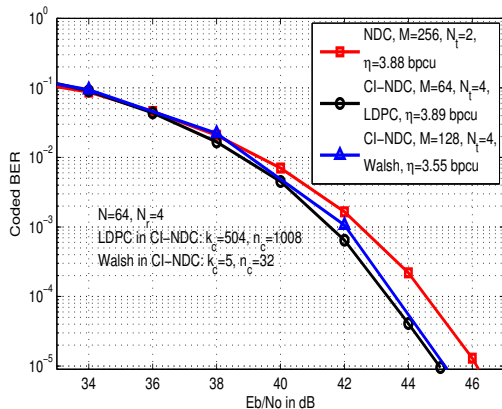


Figure : BER performance of CI-NDC OFDM and NDC OFDM at  $\eta = 3.8$  bpcu,  $N_r = 4$

- CI-NDC OFDM performs better than NDC OFDM

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## Quad-LED & dual-LED complex modulation

# Quad-LED complex modulation (QCM)

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- A complex modulation scheme for VLC
- Uses 4 LEDs (hence the name 'quad')
- Does not need Hermitian symmetry
- QCM signaling
  - LEDs are simultaneously intensity modulated by the magnitudes of the real and imaginary parts of a complex symbol
  - Sign information is conveyed through spatial indexing of additional LEDs
- QCM module can serve as a basic building block to bring in the benefits of complex modulation to VLC

R. Tejaswi, T. Lakshmi Narasimhan, A. Chockalingam, "Quad-LED complex modulation (QCM) for visible light wireless communications" [IEEE WCNC'16 Workshop on Optical Wireless Commun.](#), Apr. 2016.



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- Mapping of complex symbol  $s = s_I + js_Q$  to LEDs activity in QCM

| Real part<br>$s_I$ | Status of LEDs                    | Imag. part<br>$s_Q$ | Status of LEDs                    |
|--------------------|-----------------------------------|---------------------|-----------------------------------|
| $\geq 0$           | LED1 emits $ s_I $<br>LED2 is OFF | $\geq 0$            | LED3 emits $ s_Q $<br>LED4 is OFF |
| $< 0$              | LED1 is OFF<br>LED2 emits $ s_I $ | $< 0$               | LED3 is OFF<br>LED4 emits $ s_Q $ |

- Example:
  - If  $s = -3 + j1$ , then  
LED1: **OFF**; LED2: **emits 3**;  
LED3: **emits 1**; LED4: **OFF**  
Corresponding QCM tx. vector is  $\mathbf{x} = [0 \ 3 \ 1 \ 0]^T$
- Note:
  - Two LEDs (one among LED1 and LED2, and another one among LED3 and LED4) will be ON simultaneously. Other two LEDs will be OFF

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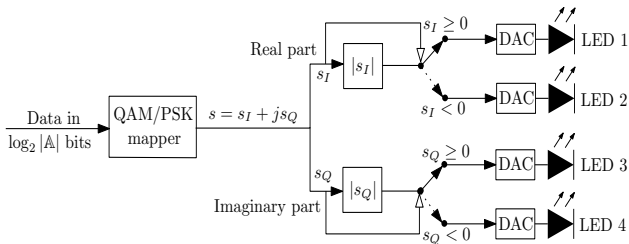
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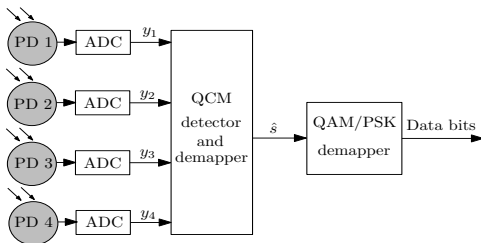
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- QCM transmitter



- QCM receiver



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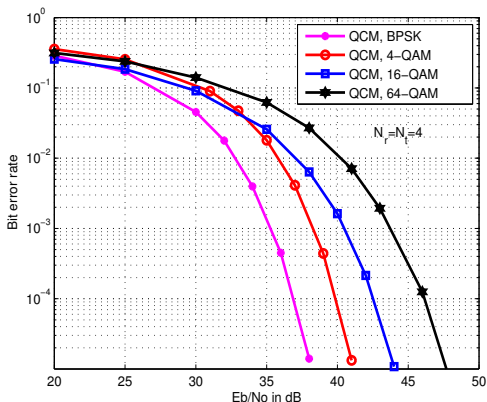
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- Crossover between performance of 4-QAM and 16-QAM
  - due to multiuser detection effect - strong interferer helps

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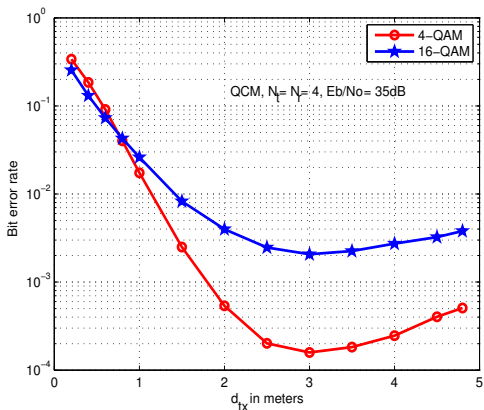
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- Effect of varying LED spacing ( $d_{tx}$ )



- optimum LED spacing
  - due to opposing effects of weak channel gain and weak channel correlation for increasing  $d_{tx}$

# QCM with phase rotation

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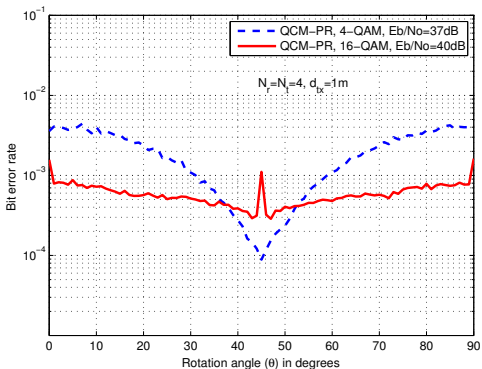
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- Rotation of complex modulation symbols
  - known to improve performance in RF wireless
- Effect of phase rotation in QCM (QCM-PR) in VLC?

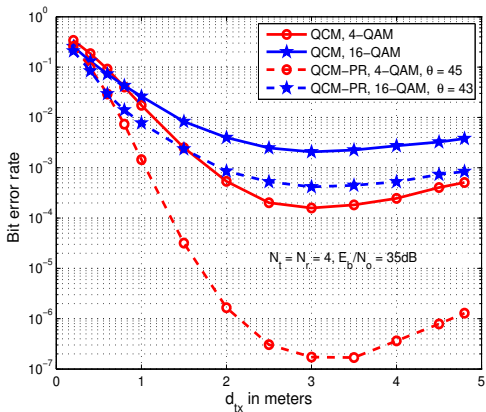


- Phase rotation helps. There is optimum rotation.

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- Performance of QCM and QCM-PR (with optimum rotation) as a function of  $d_{tx}$



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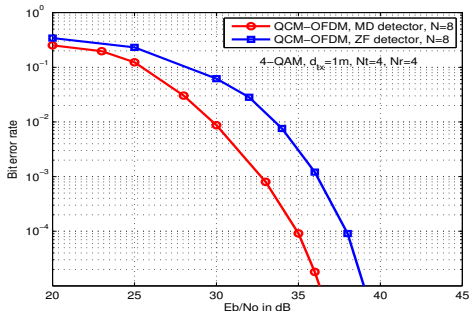
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- OFDM signaling along with QCM (QCM-OFDM)
  - $N$  complex symbols drive  $N$ -point IFFT
  - IFFT output vector (OFDM symbol) drives QCM transmitter block in  $N$  channel uses
  - QCM-OFDM signal detection
    - Zero-forcing (ZF), minimum distance (MD) detectors
  - Performance of QCM-OFDM



# QCM, QCM-PR, QCM-OFDM

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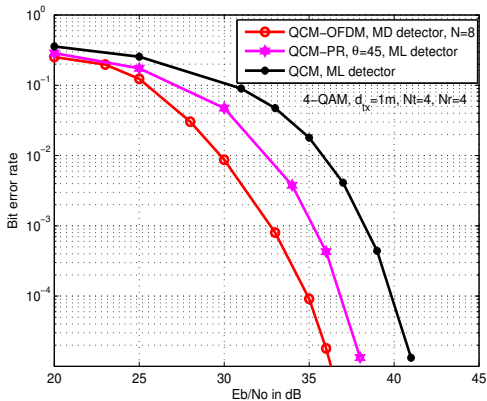
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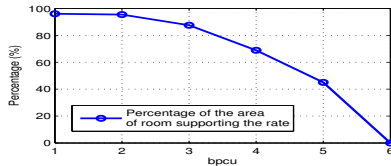
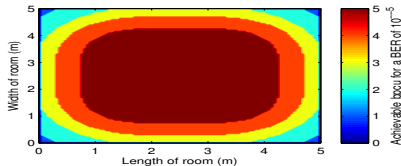
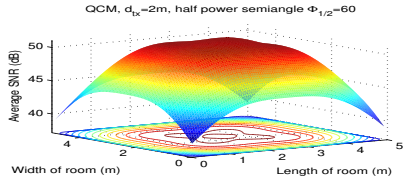
- Performance comparison between QCM, QCM-PR, QCM-OFDM





# Achievable rate contours in QCM

- Spatial distribution of received SNR
- Achievable rate (in bpcu) for a given target BER (e.g.,  $10^{-5}$  BER)
- Percentage area of the room covered vs achieved rate



# Dual-LED complex modulation (DCM)

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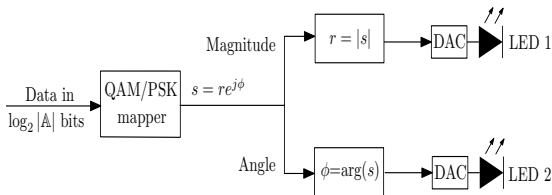
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- Exploit representation of complex symbols in **polar coordinates**
- Adequate to convey **only the magnitude and phase** of a complex symbol  $s = re^{j\phi}$ ,  $r \in \mathbb{R}^+$ ,  $\phi \in [0, 2\pi)$ 
  - only two LEDs suffice
  - no sign information to convey
- The  $2 \times 1$  DCM tx. vector is  $\mathbf{x} = [r \ \phi]^T$
- **DCM transmitter:**



T. Lakshmi Narasimhan, R. Tejaswi, and A. Chockalingam, "Quad-LED and Dual-LED complex modulation for visible light communications" [arXiv:1510.08805v2 \[cs.IT\]](https://arxiv.org/abs/1510.08805v2) 2 May 2016.

- DCM signal detection

- The  $N_r \times 1$  received signal vector is

$$\mathbf{y} = r\mathbf{H}\mathbf{x} + \mathbf{n}$$

- ML estimate of the transmit vector  $\mathbf{x}$  is

$$\hat{\mathbf{x}}_{ML} = \underset{\mathbf{x} \in \mathbb{S}_D}{\operatorname{argmin}} \|\mathbf{y} - r\mathbf{H}\mathbf{x}\|^2$$

$\mathbb{S}_D$ : DCM signal set (all possible tx. vectors  $\mathbf{x}$ )

- $\hat{\mathbf{x}}_{ML}$  is demapped to corresponding complex symbol  $\hat{s}_{ML}$
  - $\hat{s}_{ML}$  is demapped to get corresponding information bits
- Remark on DCM with  $M$ -PSK:
    - Only phase carries information in  $M$ -PSK (constant  $r$ )
      - 'magnitude-LED' becomes redundant
    - Can be viewed a single-LED scheme with  $M$ -PAM
    - Both LEDs matter when  $M$ -symbols undergo some pre-processing (e.g., IFFT in DCM-OFDM)

# Performance of QCM and DCM

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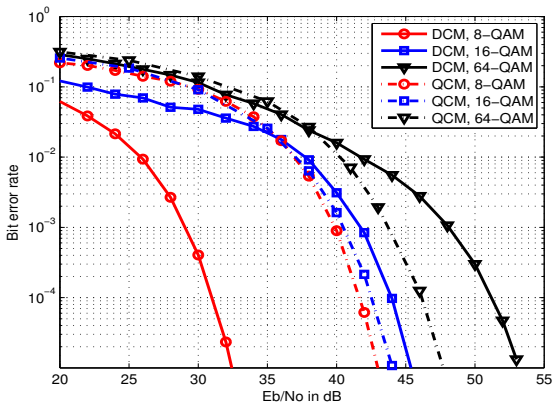
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- For small sized QAM (8-QAM), DCM performs better than QCM
- For larger sized QAM (16-QAM, 64-QAM), QCM performs better

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| Modulation alphabet | DCM     | QCM     | QCM-PR  |
|---------------------|---------|---------|---------|
| 8-QAM               | 29.2 dB | 39.8 dB | 39.2 dB |
| 16-QAM              | 41.8 dB | 40.6 dB | 38.6 dB |
| 32-QAM              | 45.5 dB | 41.8 dB | 40 dB   |
| 64-QAM              | 48.2 dB | 43.7 dB | 40.2 dB |

Table : Comparison of  $E_b/N_0$  required by DCM, QCM, and QCM-PR to achieve a BER of  $10^{-3}$  for different  $M$ -QAM alphabets.

# Performance of QCM-OFDM and DCM-OFDM

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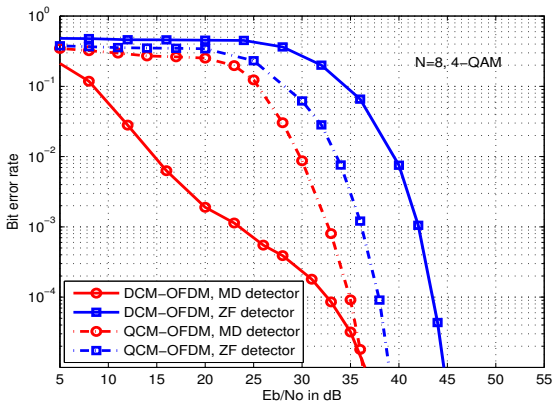
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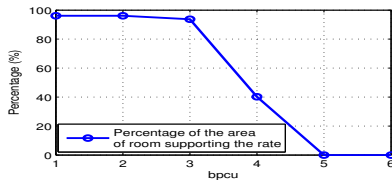
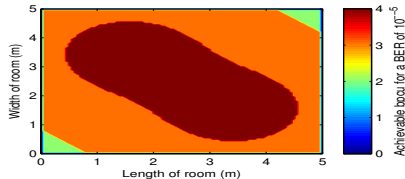
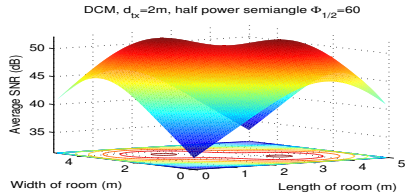
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# VLC with dimming support

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- Human eye perceives the **average intensity** (when intensity changes faster than 200 Hz)
- Need dimming support in lighting applications
  - dimming target (e.g., 75%, 50%, 25%)
- Two approaches
  - **time-domain (TD) approach**
    - adds compensation symbols of two levels (ON/OFF) within a max. flickering time period (MFTP) to match dimming target
    - **Adv:** easy to implement; **Disadv:** rate loss
  - **intensity-domain (ID) approach**
    - changes the intensity levels; also includes bias scaling (alters DC bias level), intensity distribution adaptation
    - **Adv:** high rate; suited for multi-level modulation like PAM
    - **an optimization problem formulation**
      - maximize rate w.r.t intensity level distribution

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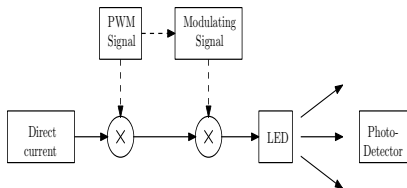
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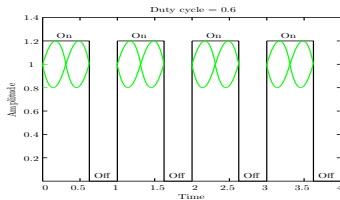
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- Data modulation (e.g., using OFDM) with dimming control (e.g., using PWM)



(a)



(b)

Z. Wang, W-D. Zhong, C. Yu, J. Chen, C. P. S. Francois, and W. Chen, **Performance of dimming control scheme in visible light communication system**, *Optics Express*, vol. 20, no. 17, pp. 18861-18868 (2012).

T. D. C. Little and H. Elgala, **Adaptation of OFDM under visible light communications and illumination constraints**, *Asilomar Conf. Signals, Systems, and Computers*, pp. 1739-1744, 2014.

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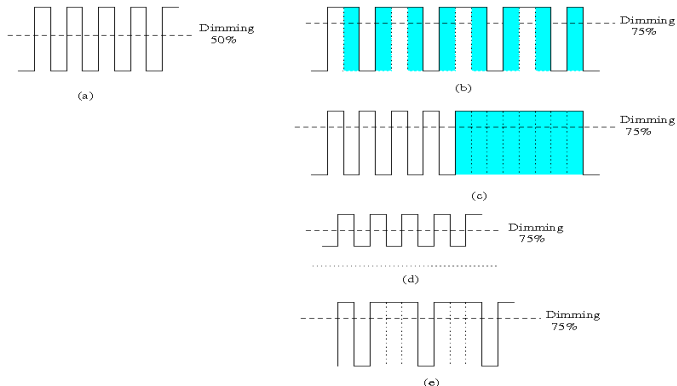
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- Examples of dimming support
  - TD approach: (b) intra-pulse insertion; (c) inter-pulse padding (IEEE 802.15.7 OOK mode uses this)
  - ID approach: (d) bias-scaling; (e) distribution adaptation



# VLC with dimming support

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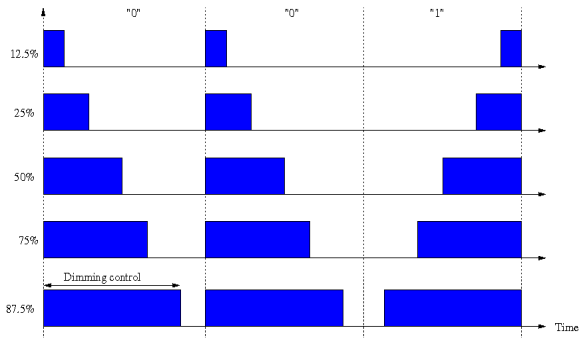
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- PPM to support dimming control



- other PPM variants (MPPM, OPPM, VPPM)

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- Vehicular communication (**intelligent transportation systems**)
  - a **challenging and challenging outdoor VLC application**
  - vehicle-to-vehicle (V2V), infrastructure-to-vehicle (I2V), vehicle-to-infrastructure (V2I)
  - Outdoor VLC elements: traffic lights, street lights, head/tail lights, etc.
- Motivation: **road-safety**; reduce road accidents
- **Typical requirements**
  - Indoor applications:
    - High data rates (Mbps-Gbps)
    - Short range (1-2 m)
  - Vehicle (outdoor) applications:
    - Relatively low data rates (Kbps)
    - Longer range (80-100 m)
    - Robustness to numerous sources of parasitic light (vehicular VLC channel is extremely noisy)

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- IEEE 802.11p (DSRC: Dedicated Short Range Communication)
  - standard for RF wireless access in vehicular environments
  - based on IEEE 802.11a
  - 75 MHz allotted in 5.9 GHz
  - rates: 3-27 Mbps; MAC: CSMA/CA; range: up to 1 Km
- Issues in DSRC
  - high traffic densities (numerous packet collisions, delay)
- Vehicular VLC can play a complementary role to DSRC
- **IEEE 802.15.7 VLC standard - PHY I**
  - intended for outdoor, long-range, low data rate applications such as I2V and V2V communication
- VLC is still an early stage technology for usage in ITS

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- Spatial reuse
  - an efficient approach to improve spectral efficiency
- Multiple light fixtures (luminaires) installed in large indoor environments (e.g., offices, airports, hospitals)
  - provide an opportunity to set up VLC systems with dense spatial reuse
- Optical attocell network
  - use each luminaire as a small base station (BS) or access point (AP)
  - smaller cell sizes compared to RF femtocells
  - uplink connection to achieve full-duplexing
  - handovers to allow users to roam within the room or an entire building
  - co-channel interference (CCI) is a key issue



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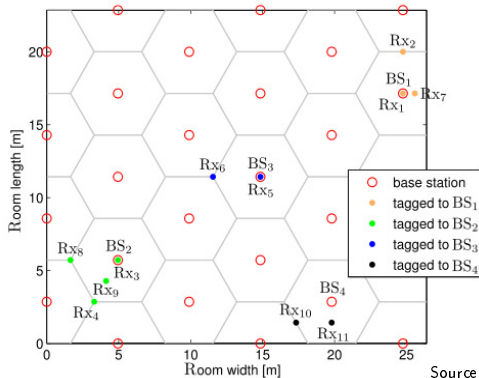
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- An example optical attocell network

- Room size: 24m  $\times$  23m  $\times$  3m
- No. of cells: 27; Cell radius: 3.3 m



Source: Ref. [1]

[1] C. Chen, S. Videv, D. Tsonev, and H. Hass, **Fractional frequency reuse in DCO-OFDM-based optical attocell networks**, *Jl. of Lightwave Tech.*, vol. 33, no. 19, pp. 3989-4000, Oct. 2015.

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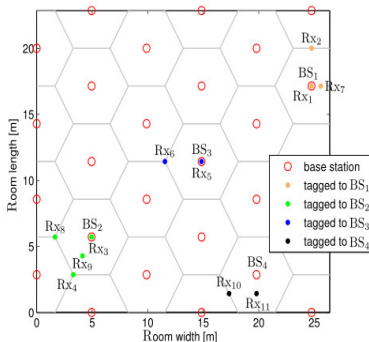
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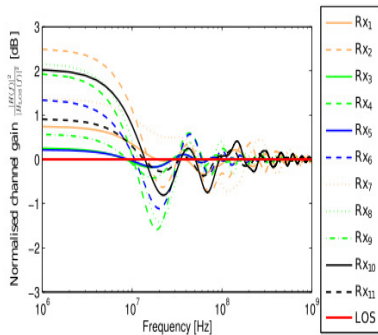
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- Channel response at different receiver locations



(c)



(d)

Source: Ref. [1]

- Receivers near walls have more variation (3 dB) than receivers far off from walls (1.5 dB)
- This is because of the strong 1st order reflections by walls
- Adaptive bit loading in OFDM can compensate for this variation

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- CCI mitigation in optical attocell networks
  - resource partitioning
  - use of different wavelengths in adjacent cells
  - interference coordination based on busy-burst signaling
  - fractional frequency reuse
    - offers good balance between average spectral efficiency, cell edge performance, system complexity
- Fractional frequency reuse (FFR)
  - strict FFR
    - one common sub-band (for cell center users)
    - multiple protected sub-bands (for cell edge users)
  - soft frequency reuse (SFR)
    - different sub-band for cell edge users in each adjacent cell
    - allows center users to take edge users' sub-bands in adjacent cells

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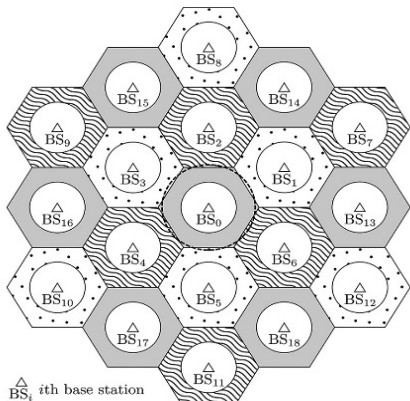
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- FR pattern in two-layer optical attocell network model
  - pattern in edge regions: reuse factor 3



Source: Ref. [1]

- Shown to be a good model to use to estimate interference statistics and user performance in attocells

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- Visible light wireless communication
  - an emerging and promising complementary technology to RF communication technology
- Several **hard-to-resist** advantages
  - with matching challenges
- A fast growing area with great potential
- MIMO and OFDM techniques for VLC are promising
- QCM and DCM: simple and novel signaling for VLC
- **Open areas for research and innovation**
  - New VLC signaling schemes
  - Outdoor VLC issues (robustness, range, rate)
  - VLC networking issues (MAC, coverage, mobility, handovers in attocells)
- **Bright future** for VLC!

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# Thank you