# On the Bit Error Performance of OTFS Modulation using Discrete Zak Transform

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Abstract-In orthogonal time frequency space (OTFS) modulation, Zak transform approach is a natural approach for converting information symbols multiplexed in the DD domain directly to time domain for transmission, and vice versa at the receiver. Past research on OTFS has primarily considered a twostep approach where DD domain symbols are first converted to time-frequency domain which are then converted to time domain for transmission, and vice versa at the receiver. The Zak transform approach can offer performance and complexity benefits compared to the two-step approach. This paper presents an early investigation on the bit error performance of OTFS realized using discrete Zak transform (DZT). We develop a compact DD domain input-output relation for DZT-OTFS using matrix decomposition that is valid for both integer and fractional delay-Dopplers. We analyze the bit error performance of DZT-OTFS using pairwise error probability analysis and simulations. Simulation results show that 1) both DZT-OTFS and two-step OTFS perform better than orthogonal frequency division multiplexing (OFDM), and 2) DZT-OTFS achieves better performance compared to two-step OTFS over a wide range of Doppler spreads.

Index Terms—Discrete Zak transform, OTFS modulation, delay-Doppler domain, diversity order, two-step OTFS.

## I. Introduction

As we rapidly progress towards the next-generation wireless technologies, i.e., 6G and beyond, the air interface and the modulation waveform must cater to diverse scenarios and use cases, which include high-Doppler wireless environments that result in rapidly time-varying channels. Orthogonal time frequency space (OTFS) modulation has gained attention due to its ability to enable highly reliable communication over high-Doppler channels [1]- [6]. OTFS modulation utilizes the delay-Doppler (DD) domain to mount information-carrying symbols. Also, it represents the time-varying channel in the DD domain, which is almost time-invariant and sparse.

In wireless communication based signal processing applications, Zak transform [7] is emerging as an important tool for directly transforming a signal in time domain to delay-Doppler (DD) domain and vice versa. In the context of OTFS modulation, Zak transform approach provides a natural means to directly convert the information symbols multiplexed in the DD domain to time domain for transmission, and vice versa at the receiver. Whereas past research on OTFS has mainly considered a two-step approach for DD domain to time domain conversion and vice versa. In the two-step approach,

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information symbols in the DD domain are converted to time-frequency (TF) domain using inverse symplectic finite Fourier transform (ISFFT) which are then converted to time domain for transmission using Heisenberg transform. Corresponding inverse transforms are carried out at the receiver to convert the received time domain signal to DD domain in two steps.

While the two-step approach has been inspired by its compatibility with existing multicarrier modulation waveforms (e.g., orthogonal frequency division multiplexing (OFDM)) and a majority of the existing work on OTFS consider this approach, the Zak approach remains less explored so far. Consequently, this paper focuses on the Zak approach and its performance in comparison with that of the two-step approach. The Zak approach in continuous time has been derived from first principles in [8], where it is shown that the spectral efficiency performance of the Zak approach remains invariant to user velocity, whereas it degrades in OFDM as the velocity increases. However, [8] does not provide a discrete-time system model for the Zak approach and the bit error rate (BER) performance. The work in [11] considers the Zak approach only at the receiver while using a two-step approach at the transmitter, and presents the BER performance. Recently, [10] has presented a discrete Zak transform (DZT) approach both at the transmitter and receiver, but it does not provide the BER performance. Also, it does not provide a compact input-output relation in a matrix-vector form amenable for BER performance evaluation. In the above context, the new contributions in this paper can be summarized as follows.

- We first develop a compact DD domain input-output relation in matrix-vector form for DZT-OTFS (with Zak approach at the transmitter as well as the receiver) using matrix decomposition that is valid for both integer and fractional delay-Dopplers. This compact vectorized input-output relation is an useful contribution as it enables the BER performance evaluation (through analysis and simulations) and the development of techniques and algorithms for DZT-OTFS transceivers.
- Using the developed vectorized input-output relation, we analyze the asymptotic diversity of DZT-OTFS. We also present the simulated BER performance of DZT-OTFS in comparison with that of the two-step approach of OTFS as well as OFDM over a range of Doppler spreads.
- Our simulation results show that i) both DZT-OTFS and two-step OTFS perform better than OFDM, and ii) DZT-OTFS achieves better performance compared to two-step OTFS over a wide range of Doppler spreads.

Notations: Matrices and vectors are denoted by upper and lower case boldface letters, respectively,  $\operatorname{diag}\{v_i\}$  denotes a diagonal matrix with diagonal entries  $v_i, i=1,2,\cdots$ , and  $\mathbf{I}_K$  denotes the identity matrix of size K.  $(\cdot)_N$  denotes the modulo N operation. Hermitian, transpose, and conjugation operations are denoted by  $(\cdot)^H$ ,  $(\cdot)^T$ , and  $(\cdot)^*$ , respectively. Hadamard product, kronecker product, and convolution operations are denoted by  $\odot$ ,  $\otimes$  and  $\otimes$ , respectively.

# II. DZT-OTFS SYSTEM MODEL

In this section, we present the DZT-OTFS system model and develop the compact DD domain input-output relation in matrix-vector form. Figure 1 shows the block diagram of a DZT-OTFS transceiver. OTFS is a two-dimensional modulation technique that uses a DD grid to multiplex information symbols from a modulation alphabet  $\mathbb{A}$ . In OTFS using DZT, KL information symbols, denoted by  $Z_x[k,l]\mathbf{s}$ , are multiplexed over a  $K\times L$  DD grid given by  $\left\{\left(k\Delta\nu=\frac{k}{KLT_s},l\Delta\tau=lT_s\right),k=0,\cdots,K-1,l=0,\cdots,L-1\right\}$ , where  $T_s=1/B$  is the symbol duration, B is the bandwidth available for communication, and  $\Delta\tau$  and  $\Delta\nu$  are the delay and Doppler resolutions, respectively. The DD domain symbols,  $Z_x[k,l]\mathbf{s}$ , are converted to TD using inverse DZT (IDZT) [10], as

$$x[n] = \frac{1}{\sqrt{K}} \sum_{k=0}^{K-1} Z_x[k, n \text{ mod } L] e^{j2\pi \frac{\lfloor n/L \rfloor}{K} k}.$$
 (1)

To mitigate the inter-frame interference, a cyclic prefix (CP) of length  $N_{CP} \geq \lceil \tau_{\max}/T_s \rceil$  is added in the TD, where  $\tau_{\max}$  is the maximum delay spread of the channel and  $\lceil \cdot \rceil$  denotes the ceil function. The TD sequence is then mounted on the time-shifted transmit pulse  $g_{tx}(t), 0 \leq t \leq T_s$ , resulting in a continuous time signal  $x_t(t)$ , given by

$$x_t(t) = \sum_{n=0}^{N+N_{CP}-1} x[(n-N_{CP})_N]g_{tx}(t-nT_s), \quad (2)$$

where  $0 \le t \le (N + N_{CP})T_s$  and N = KL. This operation is carried out in the digital-to-analog converter (DAC) block in Fig. 1. The transmitted signal  $x_t(t)$  passes through a time-varying channel whose DD domain response is given by [5]

$$h(\tau, \nu) = \sum_{i=1}^{P} h_i \delta(\tau - \tau_i) \delta(\nu - \nu_i), \tag{3}$$

where P denotes the number of resolvable paths in the DD domain,  $h_i$  is the channel gain of the ith path, and  $\tau_i = (\alpha_i + a_i)T_s$  is the delay associated with the ith path, where  $\alpha_i$  is integer part and  $a_i \in [-0.5, 0.5]$  is the fractional part of the ith path's delay. Similarly,  $\nu_i = \frac{(\beta_i + b_i)}{KLT_s}$  is the Doppler associated with the ith path, where  $\beta_i$  is integer part and  $b_i \in [-0.5, 0.5]$  is the fractional part of the ith path's Doppler. The received time domain signal is given by

$$r(t) = \int_{\nu} \int_{\tau} h(\tau, \nu) x_t(t - \tau) e^{j2\pi\nu(t - \tau)} d\tau d\nu + w(t).$$
 (4)

Substituting (2) and (3) in (4), we have

$$r(t) = \sum_{i=1}^{P} h_i \sum_{n=0}^{N+N_{CP}-1} x[(n-N_{CP})]$$

$$g_{tx}(t-\tau_i - nT_s)e^{j2\pi\nu_i t} + w(t), \qquad (5)$$

where w(t) is the additive noise. At the receiver, after matched filtering with receive pulse  $g_{rx}(t)$ , we get

$$y_t(t) = \int_{\tau} r(\tau) g_{rx}^*(t - \tau) d\tau.$$
 (6)

Let  $g_{tx}(t) = g_{rx}(t) = p(t)$ . Substituting (5) in (6), we get

$$y_t(t) = \sum_{i=1}^{P} h_i \sum_{n=0}^{N+N_{CP}-1} x[(n-N_{CP})_N]$$
$$\int_{\tau} p(\tau - \tau_i - nT_s) p^*(t-\tau) e^{j2\pi\nu_i \tau} + v(t), \quad (7)$$

where v(t) is the match filtered noise. Assuming the pulse bandwidth to be much larger than the maximum Doppler, the integral in (7) can be approximated as [10]

$$\int_{\tau} p(\tau - \tau_i - nT_s) p^*(t - \tau) e^{j2\pi\nu_i\tau} d\tau \approx e^{j2\pi\nu_i(\tau_i + nT_s)} g(t - \tau_i - nT_s), \tag{8}$$

where  $g(t) \triangleq \int_{\tau} p(\tau) p^*(t-\tau) d\tau$ . For example, g(t) for a raised cosine (RC) pulse with a roll-off factor  $\gamma$  is given by

$$g(t) = \frac{\sin(\pi t/T_s)\cos(\gamma \pi t/T_s)}{(\pi t/T_s)(1 - (2\gamma t/T_s)^2)}.$$
 (9)

The output of the matched filter is sampled at  $t=mT_s$ ,  $m=0,1,2,\cdots$ . The first  $N_{CP}$  samples corresponding to the CP are discarded. The resulting discrete time-domain signal is given by

$$y[m] = \sum_{i=1}^{P} h_i \sum_{n=0}^{N-1} x[n]g[(m-n)T_s - \tau_i]e^{j2\pi\nu_i(\tau_+ nT_s)} + v[m].$$
(10)

Substituting for  $\tau_i$  and  $\nu_i$  in (10), we get

$$y[m] = \sum_{i=1}^{P} h_i e^{j2\pi\tau_i \nu_i} \sum_{n=0}^{N-1} x[n] e_i[n] g_i[m-n] + v[m], \quad (11)$$

where  $g_i[n]=g[n-l_i]$  and  $e_i[n]=e^{j2\pi\frac{k_i}{KL}n}, n=0,\cdots,N-1,$   $l_i=\alpha_i+a_i$  and  $k_i=\beta_i+b_i$ . Here,  $g_i$  and  $e_i$  are the discrete sequences that capture the effect of delay and Doppler of the ith path in the channel, respectively. Let  $h_i'=h_ie^{j2\pi\tau_i\nu_i}$  and

$$y_i[m] = \sum_{n=0}^{N-1} x[n]e_i[n]g_i[m-n].$$
 (12)

Then (11) can be written as

$$y[m] = \sum_{i=1}^{P} h'_{i} y_{i}[m] + v[m].$$
 (13)

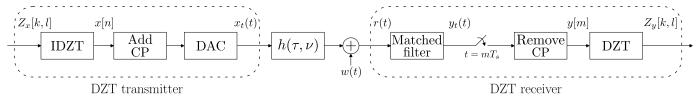


Fig. 1: Block diagram of DZT-OTFS transceiver.

# A. Vectorized formulation of DD domain input-output relation

Here, we first write the TD input-output relation in (13) in a vectorized form and transform it to a DD domain input-output relation in vectorized form using matrix decomposition as follows. The relation between  $y_i[m], x[m], e_i[m]$ , and  $g_i[m]$  can be expressed in vector form as

$$\mathbf{y}_i = (\mathbf{x} \odot \mathbf{e}_i) \circledast \mathbf{g}_i, \tag{14}$$

where  $\mathbf{y}_i, \mathbf{e}_i, \mathbf{g}_i \in \mathbb{C}^{1 \times N}$  are obtained by stacking the elements  $y_i[m], e_i[m]$  and  $g_i[m]$ , respectively. The input-output relation in (13) can then be written in a vectorized form as

$$\mathbf{y} = \begin{bmatrix} 1 & 1 & \cdots & 1 \end{bmatrix} \operatorname{diag}\{h'_1, \cdots, h'_P\} \begin{bmatrix} \mathbf{y}_1 \\ \vdots \\ \mathbf{y}_p \end{bmatrix} + \mathbf{v}. \quad (15)$$

The discrete time-domain signal y at the receiver is converted to the DD domain using DZT as

$$Z_y[k,l] = \frac{1}{\sqrt{K}} \sum_{n=0}^{K-1} y[l+nL] e^{-j2\pi \frac{k}{K}n}.$$
 (16)

The equivalent DD domain representations of (12) and (13) are given by

$$Z_{y_i}[k,l] = \sum_{m=0}^{L-1} \sum_{n=0}^{K-1} Z_x[n,m] Z_{e_i}[k-n,m] Z_{g_i}[k,l-m],$$
(17)

and

$$Z_{y}[k,l] = \sum_{i=1}^{P} h'_{i} Z_{y_{i}}[k,l] + Z_{v}[k,l],$$
 (18)

respectively.

Now, let  $\mathbf{Z}_{y_i}$ ,  $\mathbf{Z}_{e_i}$  and  $\mathbf{Z}_{g_i}$  denote the DZT of the sequences  $\mathbf{y}_i$ ,  $\mathbf{e}_i$  and  $\mathbf{g}_i$ , respectively. Let  $\mathbf{B}_u$  be a  $K \times K$  matrix whose jth row is

$$\mathbf{B}_{u}(j,:) = \mathbf{Z}_{e_{i}}^{T}(:,u)\mathbf{P}_{K}^{j-1},$$
(19)

where  $u=0,\cdots,L-1,\ j=0,\cdots,K-1,$  and  $\mathbf{P}_K$  is a  $K\times K$  permutation matrix. Further, define

$$\mathbf{E}_i = \operatorname{diag}\{\mathbf{B}_0, \cdots, \mathbf{B}_{L-1}\}. \tag{20}$$

Likewise, define a block matrix  $\mathbf{A} = [\mathbf{A}_1, \dots, \mathbf{A}_L]$ , where  $\mathbf{A}_u = \text{diag}\{\mathbf{Z}_{g_i}(:, u)\}$ . Let  $\mathbf{Q}_u$  be an  $N \times N$  matrix, given by

$$\mathbf{Q}_u = \mathbf{P}_L^{u-1} \otimes \mathbf{I}_K, \tag{21}$$

where  $P_L$  is an  $L \times L$  permutation matrix. Further, define

$$\mathbf{G}_{i} = \begin{bmatrix} \mathbf{A}\mathbf{Q}_{1} \\ \vdots \\ \mathbf{A}\mathbf{Q}_{L} \end{bmatrix}. \tag{22}$$

Using  $\mathbf{E}_i$  and  $\mathbf{G}_i$ , the effective channel matrix  $\mathbf{H}$  is given by

$$\mathbf{H} = \sum_{i=1}^{P} h_i' \mathbf{E}_i \mathbf{G}_i. \tag{23}$$

Vectorizing (18) using the above, we obtain end-to-end inputoutput relation in DD domain as

$$\mathbf{y}_{DD} = \mathbf{x}_{DD}\mathbf{H} + \mathbf{v}_{DD}, \tag{24}$$

where  $\mathbf{y}_{DD}, \mathbf{x}_{DD}, \mathbf{v}_{DD} \in \mathbb{C}^{1 \times N}$ , such that  $\mathbf{y}_{DD}(k+Kl) = Z_y[k,l], \ \mathbf{x}_{DD}(k+Kl) = Z_x[k,l], \ \text{and} \ \mathbf{v}_{DD}(k+Kl) = Z_v[k,l], \ \text{for} \ k=0,1,\cdots,K-1 \ \text{and} \ l=0,1,\cdots,L-1, \ \text{and} \ \mathbf{H} \in \mathbb{C}^{N \times N}$  is the end-to-end effective channel matrix in the DD domain. We use the compact matrix-vector representation of DZT-OTFS in (24) for the diversity analysis and BER simulations in the subsequent sections.

### III. DIVERSITY ANALYSIS OF DZT-OTFS

For the purpose of diversity analysis, the input-output relation in (24) can be written in an alternate form, as

$$\mathbf{y}_{DD} = \mathbf{h}\mathbf{X} + \mathbf{v}_{DD},\tag{25}$$

where **X** is a  $P \times N$  matrix defined as

$$\mathbf{X} = (\mathbf{I}_P \otimes \mathbf{x}_{DD}) \begin{bmatrix} \mathbf{G}_1 \mathbf{E}_1 \\ \vdots \\ \mathbf{G}_P \mathbf{E}_P \end{bmatrix}, \tag{26}$$

and  $\mathbf{h} = [h'_1, \cdots, h'_P]$  is a  $1 \times P$  vector. Let  $\mathbf{x}^i_{DD}$  and  $\mathbf{x}^j_{DD}$  be two distinct DD symbol vectors as defined in (24), and let the corresponding symbol matrices be  $\mathbf{X}_i$  and  $\mathbf{X}_j$ . Let  $\rho$  be the normalized signal-to-noise ratio (SNR) given by  $\rho = 1/N_0$ , where  $N_0$  is the noise power. Assuming maximum likelihood (ML) detection and perfect channel knowledge at the receiver, the conditional pairwise error probability (PEP) between  $\mathbf{X}_i$  and  $\mathbf{X}_j$  is given by

$$P(\mathbf{x}_{DD}^{i} \to \mathbf{x}_{DD}^{j} | \mathbf{h}) = P(\|\mathbf{y} - \mathbf{h}\mathbf{X}_{j}\|^{2} < \|\mathbf{y} - \mathbf{h}\mathbf{X}_{i}\|^{2})$$
$$= Q\left(\sqrt{\frac{\rho \|\mathbf{h}(\mathbf{X}_{i} - \mathbf{X}_{j})\|^{2}}{2}}\right). \quad (27)$$

System Parameters					of diffe	Minimum rank		
					2	3	4	William Tank
System-1 $K = 2, L = 2,$ $P = 2$	DD Profile-A	$\tau = [0,0]\Delta \tau$	w/o PR	32	208	-	-	1
		$\nu = [0, 1]\Delta\nu$	with PR	0	240	-	-	2
	DD Profile-B	$\tau = [0, 1]\Delta \tau$	w/o PR	0	240	-	-	2
		$\nu = [0, 1]\Delta\nu$	with PR	0	240	-	-	2
System-2 K = 2, L = 4, P = 4	DD Profile-C	$\tau = [0, 0, 1, 1]\Delta\tau$	w/o PR	0	136	2072	63072	2
		$\nu = [0, 1, 0, 1] \Delta \nu$	with PR	0	0	0	65280	4
	DD Profile-D	$\tau = [0.2, 1.4, 2.3, 3.6]\Delta\tau$	w/o PR	0	0	0	65280	4
		$\nu = [-0.3, 1.4, 0.8, -0.2]\Delta\nu$	with PR	0	0	0	65280	4

TABLE I: Rank profile of the difference matrices.

Using Chernoff bound and averaging over the statistics of h, the average PEP can be bounded as

$$P(\mathbf{x}_{DD}^{i} \to \mathbf{x}_{DD}^{j}) \le \mathbb{E}_{\mathbf{h}} \left\{ \exp\left(-\frac{\rho \|\mathbf{h}(\mathbf{X}_{i} - \mathbf{X}_{j})\|^{2}}{4}\right) \right\},$$
(28)

where  $\mathbb{E}_{\mathbf{h}}$  denotes expectation operation. Assuming the elements of  $\mathbf{h}$  are independent and identically distributed complex Gaussian random variables with zero mean and variance 1/P, (28) can be simplified as [11]

$$P(\mathbf{x}_{DD}^i \to \mathbf{x}_{DD}^j) \le \prod_{l=1}^r \frac{1}{1 + \frac{\rho \lambda_{lij}}{4P}},\tag{29}$$

where r is the rank of the difference matrix  $(\mathbf{X}_i - \mathbf{X}_j)$ , and  $\lambda_{lij}$  is the eigen value of  $(\mathbf{X}_i - \mathbf{X}_j)(\mathbf{X}_i - \mathbf{X}_j)^H$ . At high SNRs, using the approximation  $1 + \frac{\rho \lambda_{lij}}{4P} \approx \frac{\rho \lambda_{lij}}{4P}$ , we can write

$$P(\mathbf{x}_{DD}^i \to \mathbf{x}_{DD}^j) \le \frac{1}{\rho^r \prod_{l=1}^r \frac{\lambda_{lij}}{4P}}.$$
 (30)

Using the above average PEP expression, an upper bound on the bit error probability,  $P_e$ , can be obtained as

$$P_{e} \leq \frac{1}{QKL \log_{2} |\mathbb{A}|} \sum_{i=1}^{Q} \sum_{j=1, j \neq i}^{Q} d(\mathbf{x}_{DD}^{i}, \mathbf{x}_{DD}^{j}) P(\mathbf{x}_{DD}^{i} \to \mathbf{x}_{DD}^{j})$$

$$= \frac{1}{QKL \log_{2} |\mathbb{A}|} \sum_{i=1}^{Q} \sum_{j=1, j \neq i}^{Q} \frac{d(\mathbf{x}_{DD}^{i}, \mathbf{x}_{DD}^{j}) \rho^{-r}}{\prod_{l=1}^{r} \frac{\lambda_{lij}}{4P}}, \quad (31)$$

where  $d(\mathbf{x}_{DD}^i, \mathbf{x}_{DD}^j)$  is the Hamming distance between  $\mathbf{x}_{DD}^i$  and  $\mathbf{x}_{DD}^j$ ,  $Q = |\mathbb{A}^{KL}|$ , and  $|\cdot|$  denotes the cardinality of a set. Also, a lower bound on  $P_e$  is obtained by summing the PEPs corresponding to the pairs  $\mathbf{X}_i$  and  $\mathbf{X}_j$  such that the rank of  $(\mathbf{X}_i - \mathbf{X}_j)$  is least amongst all the pairs. From (31), it is observed that the exponent of the SNR is r which is the rank of the symbol difference matrix  $(\mathbf{X}_i - \mathbf{X}_j)$  and for all  $i, j, i \neq j$  and the minimum rank dominates the overall BER. Therefore the diversity order (DO) is given by

$$DO = \min_{i,j} rank(\mathbf{X}_i - \mathbf{X}_j).$$
 (32)

We have observed through simulations that the rank profile of the difference matrices can be such that r is less than P for several  $(\mathbf{X}_i, \mathbf{X}_j)$  pairs. This means the full DD diversity of P is not always achieved. To alleviate this, phase rotation (PR) of the transmit vector  $\mathbf{x}_{DD}$  can be carried out before

transmission. That is, instead of transmitting the  $\mathbf{x}_{DD}$  vector as such, a phase rotated vector  $\tilde{\mathbf{x}}_{DD} = \boldsymbol{\Theta} \mathbf{x}_{DD}$  is transmitted, where  $\Theta$  is a PR matrix given by  $\Theta = \text{diag}\{e^{j\frac{q}{N}}\},\$  $q=0,\cdots,N-1$ . Our simulations have shown that with this PR scheme, the full diversity of P is achieved. The above observations are illustrated in Table I which shows the rank profile of difference matrices in two systems, namely System-1 with K = L = P = 2 and System-2 with K=2, L=P=4. The rank profiles for these two systems with and without PR are shown. It can be seen that, without PR, 32 out of 240 rank matrices in System-1 with DD Profile-A have rank 1 (which is less than P = 2), resulting in a diversity order of 1. Likewise, without PR, many difference matrices in System-2 with DD Profile-C have ranks 2 and 3 (which are less than P = 4). On the other hand, with PR, all the ranks are P in both the systems for all the DD Profiles-A to D, achieving the full diversity order of P. In the next section, we have verified these minimum rank based diversity orders through BER simulations.

### IV. RESULTS AND DISCUSSIONS

In this section, we first present the simulated BER results that validate the analytical BER bounds and diversity orders obtained in the previous section. We then present the simulated BER performance of DZT-OTFS for different system settings in comparison with those of two-step OTFS and OFDM.

## A. Diversity performance of DZT-OTFS

Figure 2 shows the simulated BER performance of a DZT-OTFS system with K = L = 2 and P = 2,4. A carrier frequency ( $f_c$ ) of 4 GHz and  $\nu_p$  of 3.75 kHz (hence,  $au_p = \frac{1}{\nu_p} = 0.267$  ms) are considered. The information symbols are chosen from BPSK modulation alphabet and ML detection is used at the receiver. Simulated BER curves without PR for System-1 with DD Profile-A and DD Profile-C in Table I are plotted. The corresponding upper bound and lower bound on BER are also plotted for comparison. The following observations can be made from the figure. The upper and lower bounds on BER and the simulated BER curves almost merge at high SNRs validating the analytical BER results. Also, the diversity slopes in the high SNR regime are 1 and 2, respectively, for System-1 with DD Profile-A and System-1 with DD Profile-C. These are in agreement with the diversity orders predicted according to minimum ranks shown in Table I.

Next, Fig. 3 shows the simulated BER curves without PR for 1) System-1 with DD Profile-A, 2) System-2 with

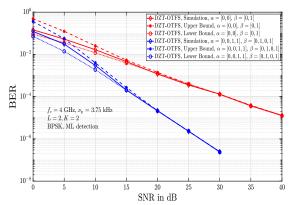


Fig. 2: Simulated BER upper and lower bounds on BER for DZT-OTFS.

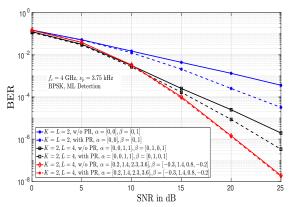


Fig. 3: BER performance of DZT-OTFS with and without PR.

DD Profile-C, and 3) System-2 with DD Profile-D. The corresponding BER curves with PR are also plotted. It is observed that the diversity slopes of the BER curves are in accordance with the minimum ranks shown in Table I. It is also observed that full diversity of P is achieved with PR.

### B. BER performance of DZT-OTFS

Here, we present the BER performance of DZT-OTFS for different system settings. The number of delay bins L and the number of Doppler bins K are chosen to meet the system specifications and channel constraints as follows. A fundamental rectangle in the DD domain of width  $\tau_p$  and height  $\nu_p$  is chosen such that  $\tau_p\nu_p=1$ , and for a given available bandwidth (B) and delay requirement (T), K and L are chosen such that  $L=\left\lceil\frac{B}{\nu_p}\right\rceil$  and  $K=\left\lceil\frac{T}{\tau_p}\right\rceil$ . The following parameters are considered in the simulations: B=60 kHz, T=4.27 ms, and  $T_s=\frac{1}{B}=16.67\mu s$ . Fixing  $\nu_p=3.75$  kHz gives  $\tau_p=\frac{1}{\nu_p}=0.267$  ms,  $L=\left\lceil\frac{B}{\nu_p}\right\rceil=16$ , and  $K=\left\lceil\frac{T}{\tau_p}\right\rceil=16$ . Fractional delay-Dopplers are considered in all the simulations and g(t) is taken to be a RC pulse with roll-off factor  $\gamma$ . The channel is considered to have P=4 paths with uniform power delay profile. For a given maximum Doppler  $\nu_{\max}$  and maximum delay  $\tau_{\max}$ , the ith path's  $\alpha_i$  is a random integer uniformly sampled from  $\{0,1,\cdots,\alpha_{\max}\}$ ,  $a_i\in \mathrm{Unif}[-0.5,0.5]$ , where  $\alpha_{\max}=\mathrm{round}\left(\frac{\tau_{\max}}{T_s}\right)$ ,  $\mathrm{Unif}[.,.]$ 

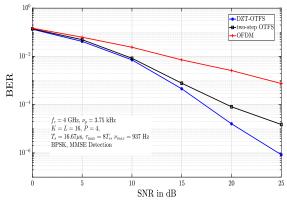


Fig. 4: BER performance of DZT-OTFS, two-step OTFS, and OFDM as a function of SNR.

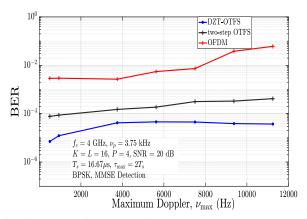


Fig. 5: BER performance of DZT-OTFS, two-step OTFS, and OFDM as a function of maximum Doppler,  $\nu_{\rm max}$ .

denotes uniform distribution, and  $\nu_i = \nu_{\rm max}\cos(\theta)$ , where  $\theta \in {\rm Unif}[-\pi,\pi]$ . The performance of two-step OTFS and OFDM are also obtained for comparison. BPSK modulation and minimum mean square error (MMSE) detection are used in all the systems.

- 1) BER as a function of SNR: Figure 4 shows the BER performance of DZT-OTFS, two-step OTFS, and OFDM as a function of SNR. The maximum delay and Doppler spreads are taken to be  $\tau_{\rm max}=8Ts=133.33~\mu{\rm s}$  and  $\nu_{\rm max}=937$  Hz, and the roll-off factor of the RC pulse  $\gamma$  is taken to be 0. From Fig. 4, it is observed that both DZT-OTFS and two-step OTFS achieve significantly better performance compared to OFDM. Also, DZT-OTFS is seen to achieve better performance compared to two-step OTFS, illustrating the inherent strength of the DZT-OTFS waveform compared to the two-step OTFS waveform. For example, at a BER of  $10^{-3}$ , DZT OTFS has an SNR gain of about 1 dB and 10 dB compared to two-step OTFS and OFDM, respectively. Further, the performance gap between DZT-OTFS and two-step OTFS increases in favor of DZT-OTFS as SNR increases.
- 2) BER as function of maximum Doppler,  $\nu_{\rm max}$ : Figure 5 shows the BER as a function of  $\nu_{\rm max}$  at an SNR of 20 dB and  $\gamma=0$ . The simulations are done for a fixed  $\tau_{\rm max}=2T_s=33.34~\mu{\rm s}$  and  $\nu_{\rm max}$  varied in the range 500

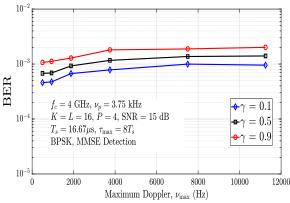


Fig. 6: Effect of RC pulse roll-off factor,  $\gamma,$  on BER vs  $\nu_{\rm max}$  performance.

Hz to 11.25 kHz. It is observed that, compared to OFDM, both DZT-OTFS and two-step OTFS are significantly more resilient to increase in maximum Doppler. In addition, DZT-OTFS is found to achieve better performance compared to two-step OTFS over a wide range of  $\nu_{\rm max}$ . This illustrates that DZT-OTFS waveform is more resilient to high Doppler spreads compared to two-step OTFS waveform.

# C. Effect of RC pulse roll-off factor

The choice of roll-off factor  $(\gamma)$  of the RC pulse plays a crucial role in the performance of DZT-OTFS. This is due to the DD domain spread of the RC pulse. As  $\gamma$  increases from 0 to 1, the spread of the RC pulse in the transform domain increases considerably. This spread of the DD domain symbols into the adjacent bins lead to a degraded BER performance. The simulation results in Figs. 6 and 7 illustrate this point, where the BER is shown as a function of  $\nu_{\rm max}$  and  $\tau_{\rm max}$ , respectively, for  $\gamma=0.1,0.5,0.9$  at an SNR of 15 dB. The performance is observed to degrade as the  $\gamma$  is increased from 0.1 to 0.9, because of the the increased spread of the RC pulse.

# D. Complexity of DZT-OTFS and two-step OTFS

Here, we present a complexity comparison between DZT-OTFS and two-step OTFS in transforming a time domain sequence to DD domain and vice-versa. For DZT-OTFS, from (16), we observe that for a given (k,l),  $Z_y[k,l]$  can be calculated for all  $k=0,1,\cdots,K-1$  using K-point discrete Fourier transform (DFT), whose complexity is  $O(K\log_2 K)$ . Therefore, for  $k=0,1,\cdots,K-1$  and  $l=0,1,\cdots,L-1$ , the overall complexity for DZT-OTFS is  $O(KL\log_2 K)$ . For two-step OTFS, transforming a signal from DD to TD via TF domain involves SFFT, whose complexity is of the order  $O(KL\log_2 KL)$ , which is higher than that of DZT-OTFS.

### V. CONCLUSIONS

In this work, we presented an early investigation of the bit error performance of OTFS modulation realized using discrete Zak transform approach. We derived a compact DD domain input-output relation for DZT-OTFS in matrix-vector form, which is valid for fractional delay-Dopplers and practical pulse shapes. This is a new and useful contribution as the derived matrix-vector representation of the end-to-end

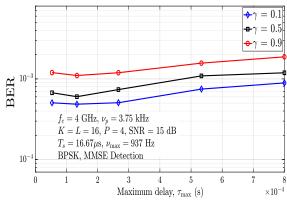


Fig. 7: Effect of RC pulse roll-off factor,  $\gamma,$  on BER vs  $\tau_{\rm max}$  performance.

DD domain input-output relation gives a basic foundation for exploring further into the design of efficient techniques and algorithms for DZT-OTFS transceivers. Our simulation results showed that DZT-OTFS can achieve better performance compared to two-step OTFS over a wide range of Doppler spreads at a lesser complexity. In this work, we presented the diversity order results through explicit computation of the rank profile of the difference matrices. A formal analytical proof on the diversity order results is a topic for future work. Also, development and performance evaluation of efficient algorithms for DD domain equalization/detection and channel estimation for DZT-OTFS remains open for future research.

# REFERENCES

- [1] R. Hadani et al., "Orthogonal time frequency space modulation," *Proc. IEEE WCNC'2017*, pp. 1-6, Mar. 2017.
- [2] S. S. Das and R. Prasad, OTFS: Orthogonal Time Frequency Space Modulation A Waveform for 6G, River Publishers, 2021.
- [3] Z. Wei et al., "Orthogonal time-frequency space modulation: a promising next-generation waveform," *IEEE Wireless Commun. Mag.*, vol. 28, no. 4, pp. 136-144, Aug. 2021.
- [4] Y. Hong, T. Thaj, and E. Viterbo, Delay-Doppler Communications: Principles and Applications, Academic Press, 2022.
- [5] P. Raviteja, K. T. Phan, Y. Hong, and E. Viterbo, "Interference cancellation and iterative detection for orthogonal time frequency space modulation," *IEEE Trans. Wireless Commun.*, vol. 17, no. 10, pp. 6501-6515, Aug. 2018.
- [6] M. K. Ramachandran and A. Chockalingam, "MIMO-OTFS in high-Doppler fading channels: signal detection and channel estimation," *Proc. IEEE GLOBECOM'2018*, pp. 206-212, Dec. 2018.
- [7] A. J. E. M. Janssen, "The Zak transform: a signal transform for sampled time-continuous signals," Philips J. Res., 43, pp. 23-69, 1988.
- [8] S. K. Mohammed, "Derivation of OTFS modulation from first principles," *IEEE Trans. Veh. Tech.*, vol. 70, no. 8, pp. 7619-7636, Aug. 2021.
- [9] S. K. Mohammed, "Time-domain to delay-Doppler domain conversion of OTFS signals in very high mobility scenarios," *IEEE Trans. Veh. Tech.*, vol. 70, no. 6, pp. 6178-6183, June 2021.
- [10] F. Lampel, A. Avarado and F. M. J. Willems, "On OTFS using the discrete Zak transform," *Proc. IEEE ICC'2022 Workshops*, pp. 729-734, May 2022.
- [11] D. Tse and P. Viswanath, "Fundamentals of Wireless Communication.", Cambridge, U.K.: Cambridge Univ. Press, 2005.